

Fig. 7.1 Parasitic turn-on for $U_{GE} = 0V$ compared with $U_{GE} = -9V$

Fig. 7.1 exemplifies the process of parasitic turn-on in a measurement of the half-bridge test configuration according to Fig. 3.9 The left picture shows clearly two collector current peaks for IGBT T_1 . The first current peak is caused by the reverse recovery current of diode D_2 , whilst the brief turn-on of IGBT T_2 causes the second current peak with a duration of approximately $50ns^4$. This additional current pulse does not pose a risk directly for the power semiconductor. However, the extra losses in the IGBT may lead to a critical temperature rise and a reduction of the lifetime. Further, oscillations are generated which may cause disruptions in the control electronics of the driver stage or the controller. Different countermeasures such as the operation with a negative voltage at the gate of IGBT T_2 will stop the parasitic turn-on under these conditions⁵.

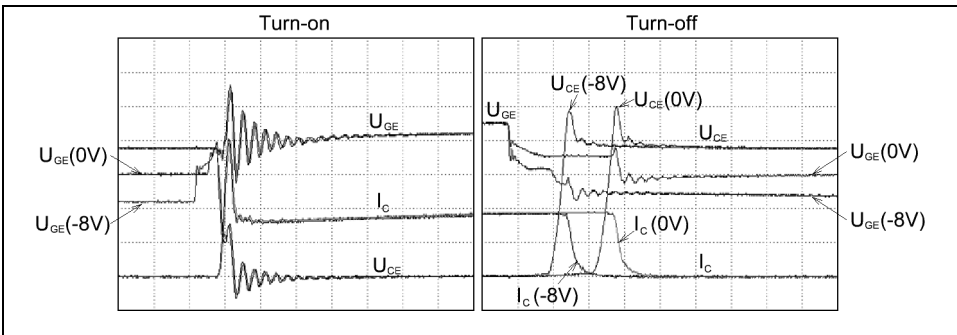


Fig. 7.2 Dependency of the IGBT switching behaviour on the control voltage U_{GE}^6

Another effect which occurs when turning off with voltages in the range of $0V$ to $-15V$ is the change of the switching times. Exemplified is this in Fig. 7.2 when turning on and off a $1.2kV$ IGBT with a gate voltage of $0V/15V$ and $-9V/15V$. The turn-on process with $0V/15V$ compared to a gate voltage of $-9V/15V$ shows a delay of approx. $200ns$ in this

⁴ Timebase here is $100ns$ per division.

⁵ IGBT T_1 is still turned on with a gate voltage of $0/15V$. In a real application, of course, both IGBTs are to be operated with the same gate voltages – in this example $-9V/15V$.

⁶ During the turn-on process the trigger point of the oscilloscope was set to the collector current I_C , while during the turn-off it depended on the gate voltage U_{GE} . The timebase is $500ns$ per division.