

# Hardware design guide for TLE92108/4

## About this document

### Scope and purpose

This application note provides information about the dimensioning of external components for the TLE92108/4 devices.

This document should be used in conjunction with the corresponding datasheet, which contains full technical details on the device specification and operation.

### Intended audience

Developers working with the TLE92108/4.

## Table of contents

<b>About this document</b> .....	<b>1</b>
<b>Table of contents</b> .....	<b>1</b>
<b>1 Introduction</b> .....	<b>2</b>
<b>2 Overview of symbols</b> .....	<b>3</b>
<b>3 Recommendation for external components</b> .....	<b>4</b>
3.1 Application diagram.....	4
3.2 External Components for the bridge driver and current sense amplifier .....	5
3.2.1 Overview of components .....	5
3.2.2 Gate driver .....	6
3.2.2.1 Gate resistors (optional) .....	6
3.2.2.2 DH low-pass filter .....	6
3.2.3 Supply voltage.....	7
3.2.4 Charge pump.....	7
3.2.5 Current sense amplifier.....	8
3.2.5.1 Current sense amplifier inputs .....	8
3.2.5.2 Current sense amplifier output .....	8
<b>4 Reverse battery protection</b> .....	<b>9</b>
<b>5 Unused pins</b> .....	<b>11</b>
<b>6 Conclusion</b> .....	<b>12</b>
<b>Revision history</b> .....	<b>13</b>

# 1 Introduction

The TLE92108/4 are Multiple MOSFET drivers, dedicated to control up to sixteen n-channel MOSFETs. They integrate eight half-bridge drivers (TLE92108), respectively four half-bridge drivers (TLE92104) for DC motor control applications such as automotive power seats, power lift gates, cargo cover, sunroof, door lock, window lifts.

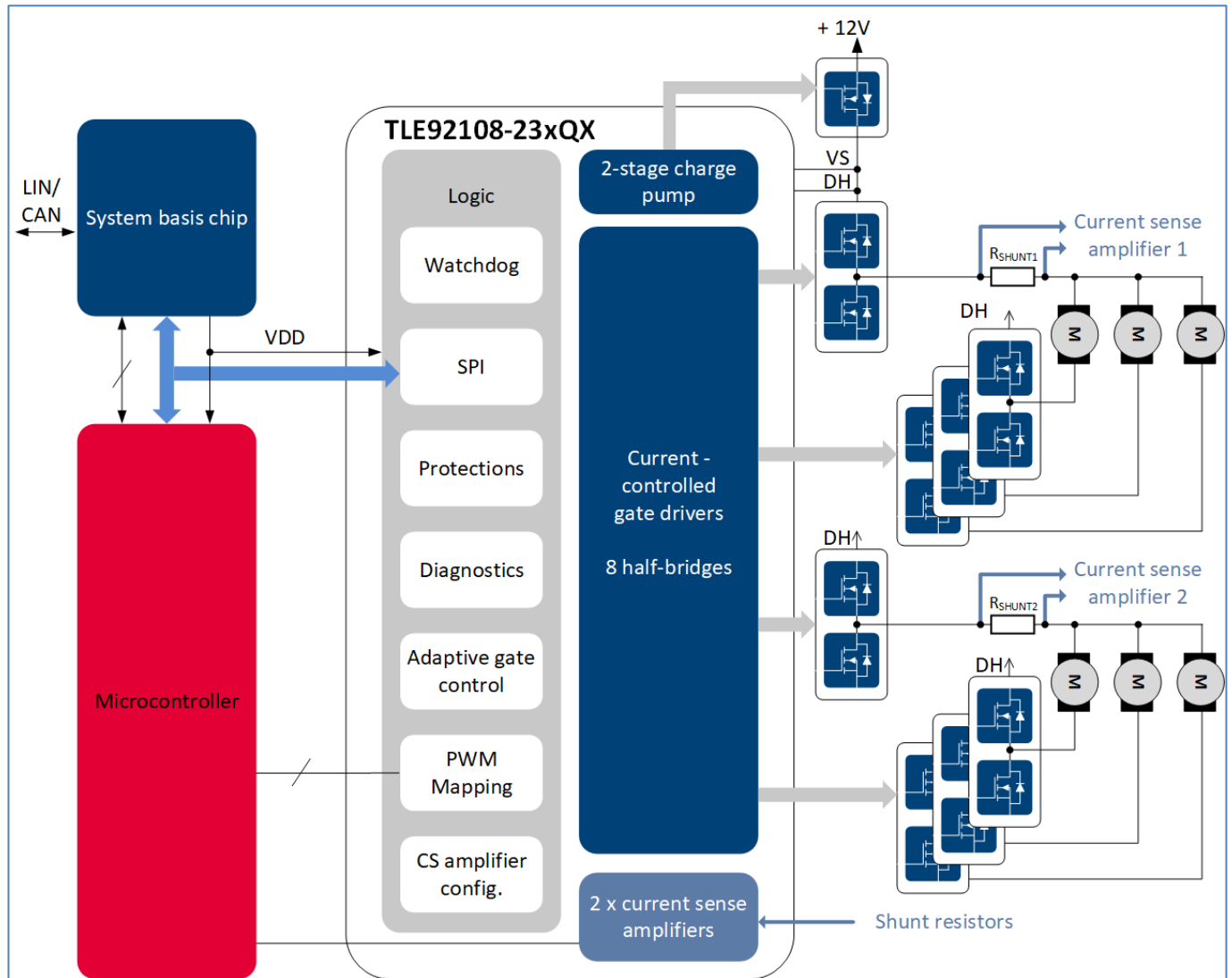


Figure 1 TLE92108 simplified block diagram in one of the possible half-bridge configurations

## 2 Overview of symbols

Symbol	Description
HB	Half bridge
DC	Direct current
CP	Charge pump
CSA	Current sense amplifier
PCB	Printed circuit board
DH	Drain input for high-sides
DS	Drain-source
HS	High side
LS	Low side

### 3 Recommendation for external components

#### 3.1 Application diagram

The following application diagram shows the gate drivers for one HB with the (partially optional) external components, which are described in this chapter.

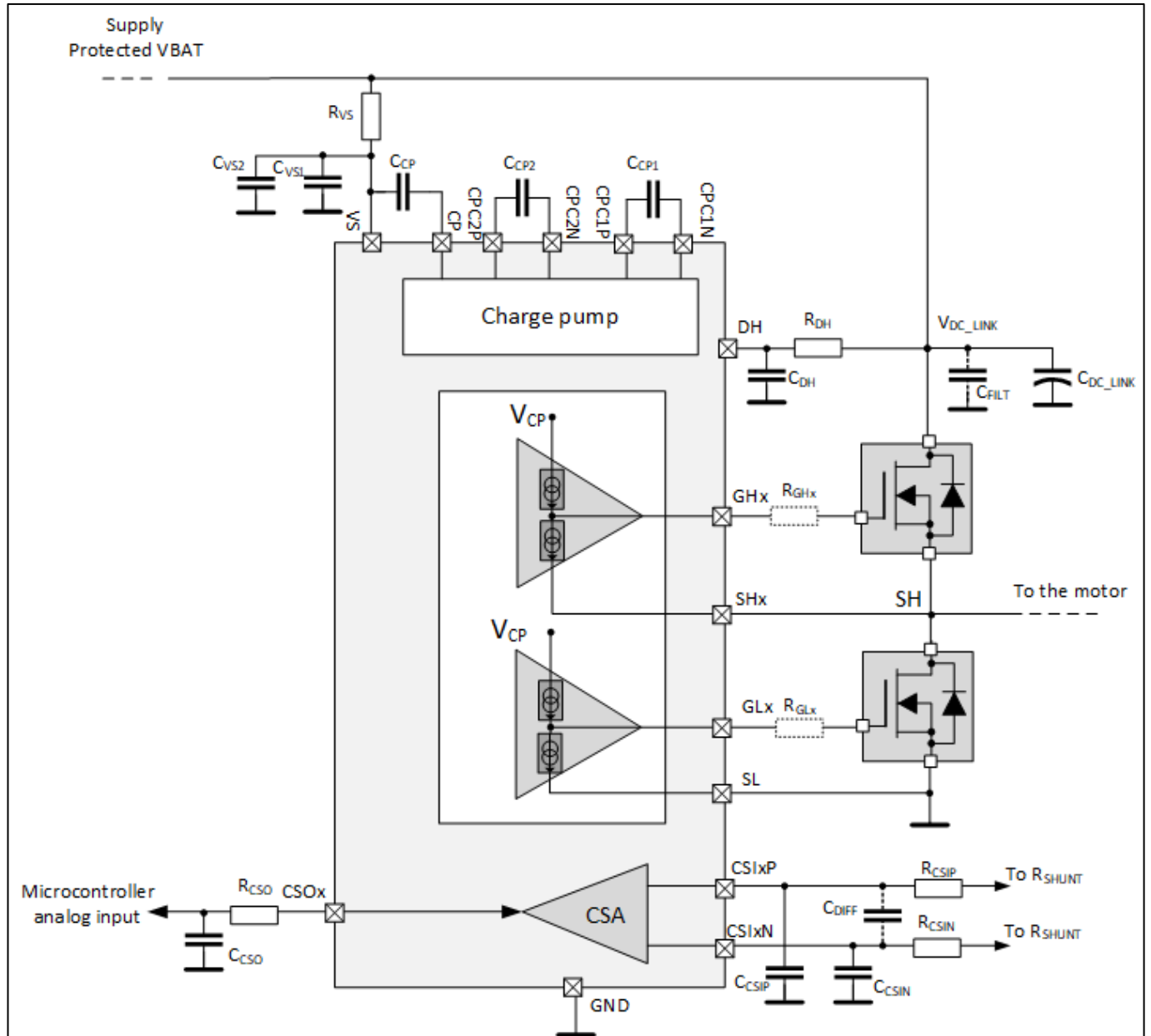


Figure 2 Gate drivers for one half bridge with external components

## 3.2 External Components for the bridge driver and current sense amplifier

### 3.2.1 Overview of components

Component	Short description	Recommended value
$R_{GHx}, R_{GLx}$	<b>Gate resistor (optional):</b> Suppresses potential oscillations between PCB line inductances and MOSFET capacitances	2 ... 10 $\Omega$
$C_{DC\_LINK}$	<b>DC link capacitor:</b> Buffers DC link voltage	Depend on application requirements
$C_{FILT}$	<b>Filter capacitor (optional):</b> Suppresses high frequency noise from the DC link voltage	
$R_{DH}, C_{DH}$	<b>Low-pass filter at VDH pin:</b> Anti-aliasing filter, suppresses high-frequency components of DC link voltage	e.g. 100 to 330 $\Omega$ , 1 nF
$R_{VS}, C_{VS1}, C_{VS2}$	<b>Low pass filter at VS pin:</b> Attenuates voltage variation at the VS pin Other functions of $C_{VS1}, C_{VS2}$ $C_{VS1}$ : Filter capacitor for high frequency noise coming from the VS pin $C_{VS2}$ : Filter capacitor for the charge pump	$R_{VS}$ : 2.2 Ohm $C_{VS1}$ : 100 nF $C_{VS2}$ : 2.2 $\mu$ F
$C_{CP}$	<b>Charge pump:</b> Buffer capacitor	470 nF
$C_{CP1}, C_{CP2}$	<b>Charge pump:</b> Flying capacitors	220 nF
$R_{CSIP}, R_{CSIN}$	<b>CSA input filter:</b> RC filter resistors necessary for noise immunity	3.3 $\Omega$
$C_{CSIP}, C_{CSIN}$	<b>CSA input filter:</b> RC filter capacitors necessary for noise immunity	22 nF
$C_{DIFF}$	<b>CSA input filter (optional):</b> Capacitor for differential filtering	1.5 nF
$R_{CSO}$	<b>CSA output filter:</b> RC filter resistor to filter high frequency noise from the motor	1 k $\Omega$
$C_{CSO}$	<b>CSA output filter:</b> RC filter capacitor to filter high frequency noise from the motor	47 nF

**Table 1 External components related to the bridge driver and the current sense amplifiers**

## 3.2.2 Gate driver

### 3.2.2.1 Gate resistors (optional)

The gate resistors  $R_{GLx}$  and  $R_{GHx}$  suppress potential oscillations between the PCB line inductances and the MOSFET capacitances. These two components can build up a LC oscillator, which can be stimulated by fast transients during the MOSFET switching. The value of  $R_{GLx}$  and  $R_{GHx}$  depend on the PCB layout, the MOSFET parasitics and the switching speed.  $R_{GLx}$  and  $R_{GHx}$  may not exceed  $10\ \Omega$ , to avoid affecting the charge and discharge currents.

**Note:** This effect is layout dependent. Such oscillations have not been observed by Infineon so far. Therefore, it is recommended to use  $0\ \Omega$  resistors for the first prototype. If no oscillations are observed, then these gate resistors can be removed for the final version of the board.

### 3.2.2.2 DH low-pass filter

The DH input pin can be configured as the reference voltage for the drain of the high-side MOSFETs, which is used for the drain-source overvoltage detection.

The low-pass filter  $R_{DH}$  and  $C_{DH}$  at the DH pin is an anti-aliasing filter which suppresses high-frequency noise from the DC link voltage.

The voltage shift between the DC link voltage and the DH pin ( $V_{DC\_LINK} - V_{DH}$ ) should be limited during the oscillation of the battery voltage. A too high voltage shift between  $V_{DC\_LINK}$  and  $V_{DH}$  can lead to a wrong DS overvoltage detection of the high-side MOSFETs.

The DS comparator of the HS MOSFETs monitors the voltage difference:

$$V_{DH} - V_{SHx} = V_{DH} - V_{DC\_LINK} + V_{DC\_LINK} - V_{SHx}$$

Where the term  $V_{DH} - V_{DC\_LINK}$  represents the voltage shift caused by the RC filter during the variation of the  $V_{DC\_LINK}$ .

It is recommended to design a RC time constant that is significantly lower than the DS monitoring filter time ( $t_{FVDS}$ ). If  $t_{FVDS} = 1 \dots 2\ \mu\text{s}$ , it is recommended to keep the RC time constant in the range of 100 to 400 ns. For example:

- $R_{DH} = 100\ \text{to}\ 330\ \Omega$
- $C_{DH} = 1\ \text{nF}$

## 3.2.3 Supply voltage

The DC link capacitors  $C_{DC\_LINK}$  and  $C_{FILT}$  are implemented in the circuitry:

- $C_{DC\_LINK}$ : a big capacitor, which works as a buffer capacitor.
- $C_{FILT}$ : a multi-layer ceramic capacitor, which suppresses high frequency noise from the DC link voltage.

The dimension of  $C_{DC\_LINK}$ :

- Depends on the allowed DC link voltage ripple caused by PWM operation, and on additional application-specific requirements. It is recommended to limit the voltage ripple to 1 V peak-to-peak.
- Must be big enough to store the motor energy in the case of an emergency shutdown of the MOSFETs when the motors is running.

It is recommended to choose capacitors with low ESR and low self-inductance.  $C_{DC\_LINK}$  and  $C_{FILT}$  should be close to corresponding HS MOSFETs to minimize stray inductances in the high-current path.

## 3.2.4 Charge pump

The charge pump is designed to supply the bridge driver integrated in the TLE9210x devices. The voltage  $V_{CP}$  is generated by a dual stage charge pump, as a multiplying effect of the input voltage  $V_S$  using two flying capacitors  $C_{CP1}$  and  $C_{CP2}$ . The capacitor  $C_{CP}$  acts as buffer capacitor between CP and  $V_S$ .

**Note:**  $C_{CP1}$  and  $C_{CP2}$  should be placed to the device as close as possible to reduce the electromagnetic emission.

It is recommended to use:

- Low ESR ceramics capacitors
- 50 V rated capacitors to minimize the DC-bias effect on the effective capacitance
- 220 nF for  $C_{CP1}$ ,  $C_{CP2}$
- 470 nF for CCP

## 3.2.5 Current sense amplifier

The Current Sense Amplifier (CSA) is an analog circuit capable to amplify the differential input voltage by a programmable gain.

### 3.2.5.1 Current sense amplifier inputs

An input filter is necessary for noise immunity. The following values are recommended:

- $R_{CSIP} = R_{CSIN} = 2.2$  or  $3.3 \Omega$ . A higher value affects the gain accuracy
- $C_{SIP} = C_{SIN} = 22$  nF
- $C_{DIFF}$  (optional) = 1.5 nF

### 3.2.5.2 Current sense amplifier output

It is recommended to use a RC filter consisting of  $R_{CSO}$  and  $C_{CSO}$  at the outputs of the current sense amplifiers (CSOx pins) to filter high frequency noise (for example caused by the motor commutations and by the charge pump switching activity).

The time constant of the filter should be at least  $4 \mu\text{s}$  in order to filter transients and noise coming from the charge pump (typ. 250 kHz).

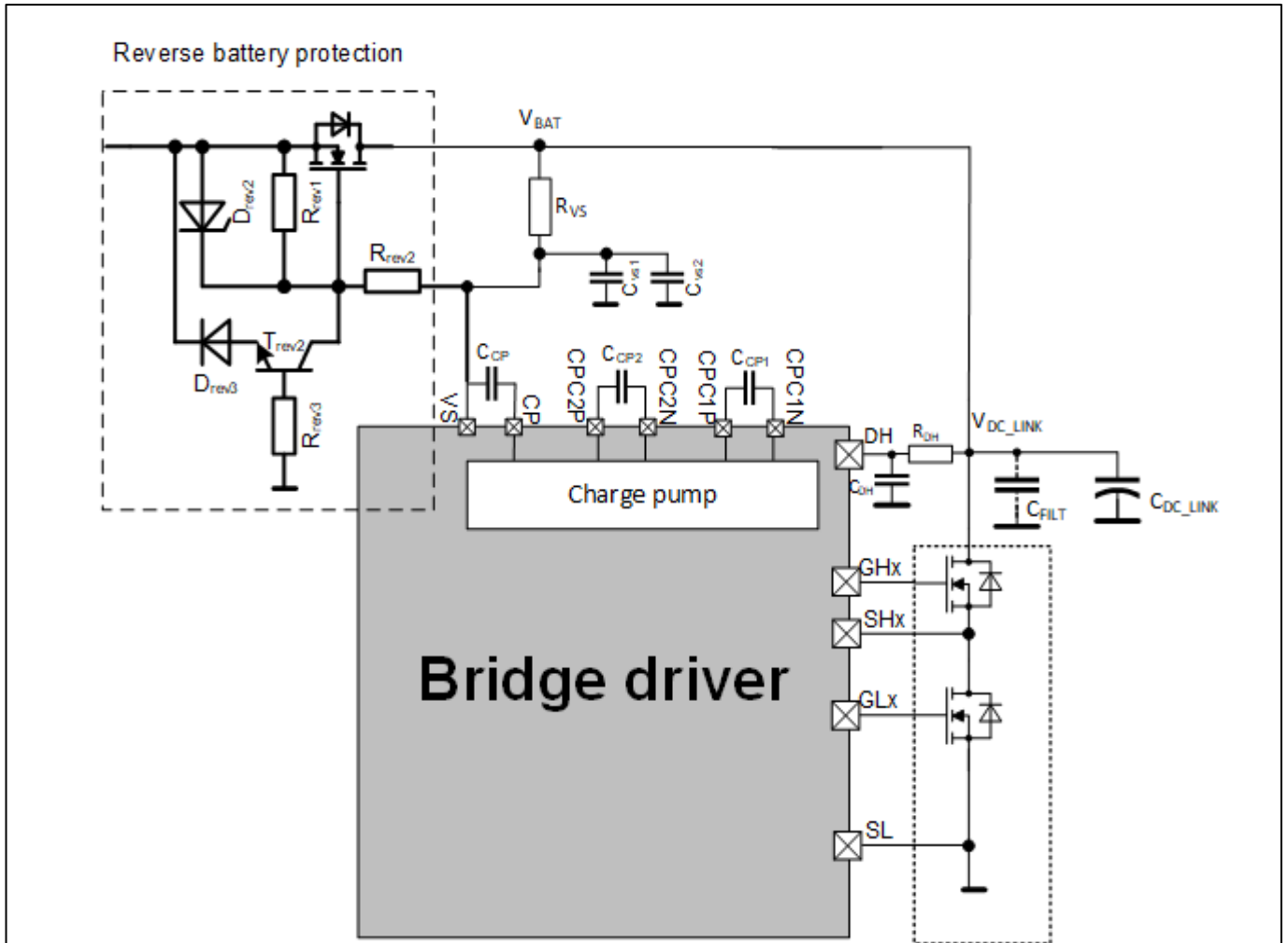
For example:

- $R_{CSO} = 1$  kOhm
- $C_{CSO} = 47$  nF



## 4 Reverse battery protection

The reverse battery protection circuit prevents the device from being damaged when the polarity of the battery is inverted.



**Figure 3 Reverse battery protection**

**When  $V_{BAT}$  is positive** and within the device operating range: the body diode of  $T_{rev1}$  supplies  $V_S$ , which is the input of the charge pump. This allows the charge pump to operate and to actively turn on  $T_{rev1}$  to minimize the power dissipation  $T_{rev1}$ .

**When  $V_{BAT}$  is negative:**  $T_{rev1}$  must be turned off by an external circuitry to protect the module

The zener diode  $D_{rev2}$  works as a gate-source overvoltage protection for  $T_{rev1}$ . The breakdown voltage of  $D_{rev2}$ :

- Should be lower than the absolute maximum rating of gate-source voltage of  $T_{rev1}$
- Is ideally higher than  $V_{CP}-V_S$  to avoid consuming current from the charge pump in normal conditions

$R_{rev1}$  prevents the gate of  $T_{rev1}$  from floating, when the CP pin is disconnected.

$T_{rev2}$ ,  $D_{rev3}$  and  $R_{rev3}$ . actively discharge the gate of  $T_{rev1}$  in case of reversed polarity connection:

- In reversed polarity conditions,  $T_{rev2}$  is turned on, ensuring a fast discharge of  $T_{rev1}$ .  $R_{rev3}$  limits the base current of  $T_{rev2}$ .
- In normal polarity conditions,  $T_{rev2}$  stays off.  $D_{rev3}$  ensures that the maximum rating of the emitter-to-basic voltage of  $T_{rev1}$  is not exceeded

$R_{rev2}$  limits the current flowing out of the CP pin in the following conditions:

- Positive battery voltage and the zener voltage of  $D_{rev2}$  is lower than  $V_{CP} - V_S$
- Reverse battery conditions, while  $T_{rev2}$  is conducting

Device	Positive battery voltage	Reverse battery conditions	Comments
$T_{rev1}$	Turned on by the charge pump	Turned by off $T_{rev2}$	The breakdown voltage of $T_{rev1}$ must be compatible to the application negative voltage
$D_{rev2}$	$T_{rev1}$ gate-source overvoltage protection		The breakdown voltage of $D_{rev2}$ must be: <ul style="list-style-type: none"> <li>- lower than the absolute maximum rating of gate-source of <math>T_{rev1}</math></li> <li>- higher than <math>V_{CP} - V_S</math></li> </ul>
$R_{rev1}$	Prevents the gate of $T_{rev1}$ from floating		100 k $\Omega$
$T_{rev2}$	OFF	Actively discharges $T_{rev1}$	–
$D_{rev3}$	Prevents current flow into the emitter of $T_{rev2}$		The breakdown voltage of $D_{rev3}$ must be must be higher than max. positive $V_{BAT}$ voltage
$R_{rev3}$		Limits the base current of $T_{rev2}$	–
$R_{rev2}$	Limits current flowing out of CP if $D_{rev2}$ breakdown	Limits current flowing out of CP when $T_{rev2}$ is conducting	4.7 k $\Omega$ recommended 3.3 k $\Omega$ minimum

**Table 2 Summary of components functions in the reverse battery protection circuitry**

## 5 Unused pins

Recommendation for unused pins:

- GHx pins: should be left open
- SHx pins: should be connected to GND. Connecting SHx to GND while the brake mode is activated avoids a wrong drain-source overvoltage detection on the not connected LSx.
- GLx pins: should be left open

## 6 Conclusion

This application note shows how to choose and dimension passive components that are necessary or good-to-have in order that the half-bridge driver, charge pump and current sense amplifier of the TLE9210x work correctly and efficiently. Besides, this document explains how the reverse battery protection circuit works and which components it consists of. Finally, it gives recommendation on configuration of unused pins.

## Revision history

Document version	Date of release	Description of changes
01.00	2021-08-11	First release
01.10	2022-07-20	Add a chapter on how to configure unused pins

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**Edition 2022-07-20**

**Published by**

**Infineon Technologies AG**

**81726 Munich, Germany**

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**Document reference**

**Z8F80186205**

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