

Automatic Gain Control (AGC)

Usage of the Automatic Gain Control Circuit

**TDA520x, TDA521x, TDA522x,
TDA7200, TDA7210 and TDA7210V**

ASK and ASK/FSK Superheterodyne Receivers (SHR) for the sub 1 GHz
frequency bands

Application Note

Revision 2.0, 2014-09-05

Edition 2014-09-05

**Published by
Infineon Technologies AG
81726 Munich, Germany**

**© 2014 Infineon Technologies AG
All Rights Reserved.**

Legal Disclaimer

The information given in this document shall in no event be regarded as a guarantee of conditions or characteristics. With respect to any examples or hints given herein, any typical values stated herein and/or any information regarding the application of the device, Infineon Technologies hereby disclaims any and all warranties and liabilities of any kind, including without limitation, warranties of non-infringement of intellectual property rights of any third party.

Information

For further information on technology, delivery terms and conditions and prices, please contact the nearest Infineon Technologies Office (www.infineon.com).

Warnings

Due to technical requirements, components may contain dangerous substances. For information on the types in question, please contact the nearest Infineon Technologies Office.

Infineon Technologies components may be used in life-support devices or systems only with the express written approval of Infineon Technologies, if a failure of such components can reasonably be expected to cause the failure of that life-support device or system or to affect the safety or effectiveness of that device or system. Life support devices or systems are intended to be implanted in the human body or to support and/or maintain and sustain and/or protect human life. If they fail, it is reasonable to assume that the health of the user or other persons may be endangered.

Automatic Gain Control (AGC)

Revision History: 2014-09-05, 1

Previous Revision: V1.1, 2010-09-07

Page	Subjects (major changes since last revision)
	Description for High Gain Mode in chapter "4.2 High Gain Mode" changed

Trademarks of Infineon Technologies AG

APOXI™, BlueMoon™, COMNEON™, CONVERGATE™, COSIC™, C166™, CROSSAVE™, CanPAK™, CIPOST™, CoolMOS™, CoolSET™, CORECONTROL™, DAVE™, EasyPIM™, EconoBRIDGE™, EconoDUAL™, EconoPACK™, EconoPIM™, EiceDRIVER™, EUPEC™, FCOS™, FALC™, GEMINAX™, GOLDMOS™, HITFET™, HybridPACK™, ISAC™, ISOFACE™, IsoPACK™, my-d™, MIPAQ™, ModSTACK™, NovalithIC™, OmniTune™, OmniVia™, OPTIVERSE™, OptiMOS™, ORIGA™, PROFET™, PRO-SIL™, PrimePACK™, RASIC™, ReverSave™, SCEPTRE™, SEROCCO™, SICOFI™, SMARTi™, SMINT™, SOCRATES™, SatRIC™, SensoNor™, SINDRION™, SmartLEWIS™, SIEGET™, TrueNTRY™, TEMPFET™, TriCore™, thinQ!™, TRENCHSTOP™, VINAX™, VINETIC™, X-GOLD™, XMM™, X-PMU™, XPOSYS™, XWAY™.

Other Trademarks

AMBA™, ARM™, MULTI-ICE™, PRIMECELL™, REALVIEW™, THUMB™ of ARM Limited, UK. AUTOSAR™ is licensed by AUTOSAR development partnership. Bluetooth™ of Bluetooth SIG Inc. CAT-ig™ of DECT Forum. COLOSSUS™, FirstGPS™ of Trimble Navigation Ltd. EMV™ of EMVCo, LLC (Visa Holdings Inc.). EPCOS™ of Epcos AG. FLEXGO™ of Microsoft Corporation. FlexRay™ is licensed by FlexRay Consortium. HYPERTERMINAL™ of Hilgraeve Incorporated. IEC™ of Commission Electrotechnique Internationale. IrDA™ of Infrared Data Association Corporation. ISO™ of INTERNATIONAL ORGANIZATION FOR STANDARDIZATION. MATLAB™ of MathWorks, Inc. MAXIM™ of Maxim Integrated Products, Inc. MICROTEC™, NUCLEUS™ of Mentor Graphics Corporation. Mifare™ of NXP. MIPI™ of MIPI Alliance, Inc. MIPS™ of MIPS Technologies, Inc., USA. muRata™ of MURATA MANUFACTURING CO. OmniVision™ of OmniVision Technologies, Inc. Openwave™ Openwave Systems Inc. RED HAT™ Red Hat, Inc. RFMD™ RF Micro Devices, Inc. SIRIUS™ of Sirius Sattelite Radio Inc. SOLARIS™ of Sun Microsystems, Inc. SPANSION™ of Spansion LLC Ltd. Symbian™ of Symbian Software Limited. TAIYO YUDEN™ of Taiyo Yuden Co. TEAKLITE™ of CEVA, Inc. TEKTRONIX™ of Tektronix Inc. TOKO™ of TOKO KABUSHIKI KAISHA TA. UNIX™ of X/Open Company Limited. VERILOG™, PALLADIUM™ of Cadence Design Systems, Inc. VLYNQ™ of Texas Instruments Incorporated. VXWORKS™, WIND RIVER™ of WIND RIVER SYSTEMS, INC. ZETEX™ of Diodes Zetex Limited.

The information in this document is subject to change without notice.

Last Trademarks Update 2009-05-27

Table of Contents

1	Introduction	6
2	AGC Active Mode	7
3	Setting the RSSI Threshold	9
4	AGC Inactive Mode	10
4.1	Low Gain Mode	10
4.2	High Gain Mode	11
5	RSSI Curves for Active and Inactive Modes	12
6	Conclusion	13

List of Figures

Figure 1	IF Output stage driving the 330 Ω impedance of the 10.7 MHz CER Filter	6
Figure 2	AGC Control Loop Block Diagram	7
Figure 3	TAGC voltage with respect to the RSSI voltage	8
Figure 4	Forcing the LNA in the low gain mode	10
Figure 5	Forcing the LNA in the high gain mode with pin 4 grounded	11
Figure 6	RSSI curves for active and inactive modes	12

1 Introduction

The TDA520x, TDA521x, TDA522x, TDA7200, TDA7210 and TDA7210V receivers provide an AGC (Automatic Gain Control) circuit that can be used in the active mode or in the inactive low gain mode to extend the dynamic range of the receiver. Since the mixer output stage has a fixed bias current of 300 μ A from a constant current source that drives the CER filter load of 330 Ohm, an IF output signal of 100mV (70 mVrms) will already start becoming nonlinear. Assuming a voltage gain of 40 to 50 dB from the antenna to the IF output, a good starting point for to enable the AGC circuit is -70...-60 dBm to avoid this nonlinearity. The action of asserting the LNA in the low gain mode will reduce the subharmonic interferers of 10.7 MHz IF. Without the AGC circuit, the current through the output of the mixer stage is starved during strong signal conditions, thus 10.7 MHz IF harmonics can be created at the IF output.

Another method to reduce the subharmonic interferer is to increase the bias current in the mixer output stage (IFO at pin-12). Increasing the bias current can be accomplished by placing a resistor from the IFO to ground. By adding a shunt resistor of 1.2 k Ω the IIP3 of the LNA and Mixer stages is increased by ~9 dB at 434 MHz for instance. Please see Figure 1.

Note: The pin numbers indicated in this document are valid for all types except the TDA7210V.

At the TDA7210V pin "TAGC" is pin 2 (pin 4 at all other types) and pin "IFO" is pin 10 (pin 12 at all other types).

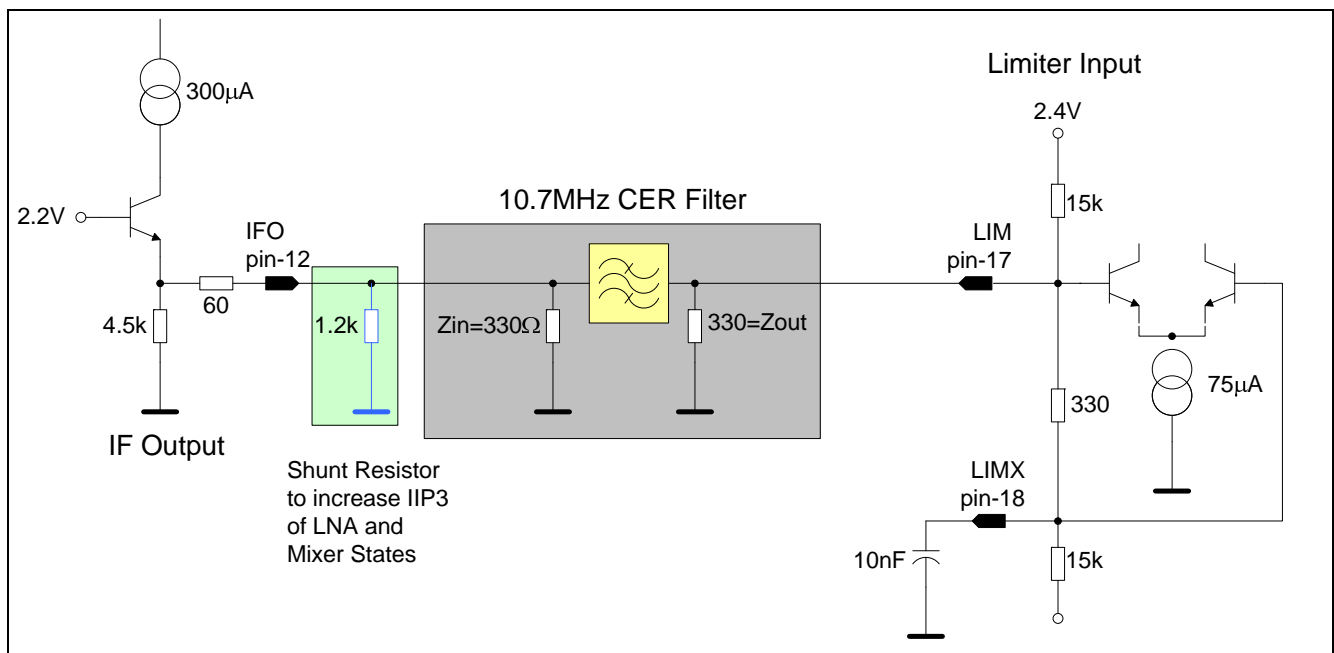


Figure 1 IF Output stage driving the 330 Ω impedance of the 10.7 MHz CER Filter

2 AGC Active Mode

In the active mode, the Receiver Signal Strength Indicator (RSSI) voltage is compared with a reference voltage applied on pin 23 of the receiver (V_{THRES}). The RSSI voltage is generated by summing current from the logarithmic Limiter Amplifier. The resulting RSSI voltage is proportional to the power applied at the Low Noise Amplifier input (LNI). The voltage for V_{THRES} can be derived from a resistor divider that uses the precision +3 V output from pin 24 of the receiver. When the RSSI signal is higher than V_{THRES} , the Operational Transconductance Amplifier (OTA) will source a current of 4.2 μA into an external capacitor at pin 4 of the receiver (TAGC), which causes a reduction of LNA gain. Whereas, a RSSI signal voltage below V_{THRES} will cause the OTA to sink current of 1.5 μA from the capacitor on TAGC keeping the LNA gain high. The relative large charge current ($RSSI > V_{THRES}$) means a fast reduction of the LNA gain, known as fast attack. The LNA gain can be reduced by maximum ~ 20 dB. The much smaller discharge current of only 1.5 μA ($RSSI < V_{THRES}$) means a slow release (much longer decay time than the attack time) that bridges logic zeros of an OOK (ASK) signal, when no RF power is received. The value of the capacitor connected to pin 4 determines the attack and decay time of the AGC and has to be adjusted according to the data rate of the received signal.

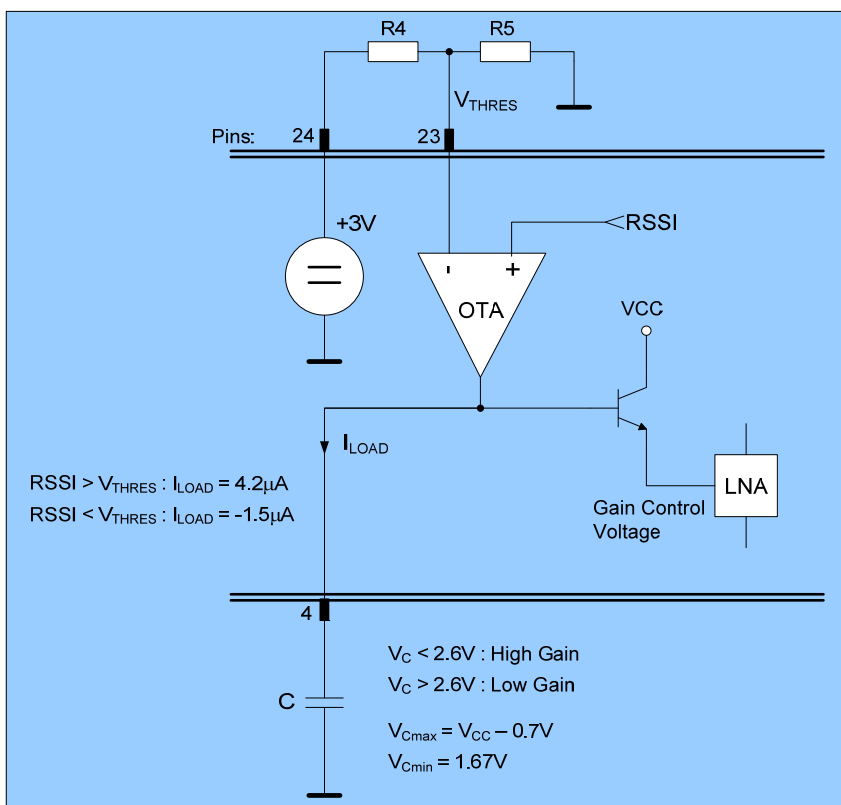


Figure 2 AGC Control Loop Block Diagram

The action of sourcing or sinking current from the OTA generates a DC voltage on the capacitor connected to pin 4 correlating to the RF input power. A voltage across the capacitor (V_{TAGC}) of less than 2.6 V forces the LNA into the high gain mode, whereas a voltage higher than 2.6 V forces the LNA into low gain mode. This is shown in Figure 3 where $V_{THRES} = 1.85$ V. When the RSSI reaches V_{THRES} (~ -83 dBm), the voltage at pin 4 (V_{TAGC}) rises to 2.6 V, which means that the AGC starts to reduce the gain of the LNA. That's why a further increase of the input level up to ~ -63 dBm does not cause a further increase of the RSSI signal. So the AGC keeps the RSSI signal almost constant over an RF input level range of ~ 20 dB by reducing the gain of the LNA up to 20 dB. Above a RF input level of -63 dBm the RSSI signal increases with the same steepness as below the threshold (in high gain mode), whereas the voltage V_{TAGC} increase to 4.4 V where it is then internally clamped. At the end of the dynamic range of the Limiter Amplifier becomes saturated and the RSSI voltage stays almost constant.

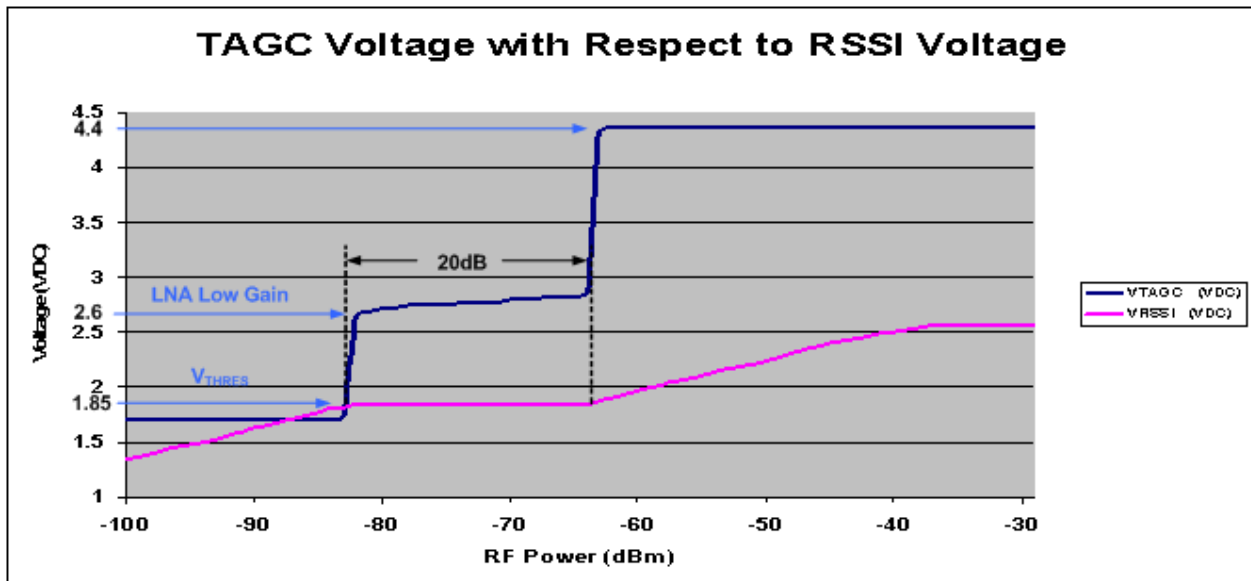


Figure 3 TAGC voltage with respect to the RSSI voltage

3 Setting the RSSI Threshold

The higher the received signal RF level the higher the SNR of the demodulator input and the lower the system noise figure of the receiver. Since the system noise figure (NF) increases, and consequently the SNR decreases with decreasing gain of the LNA, the gain of the LNA should be as high as possible for low level RF signals to achieve maximum receiver sensitivity.

Consequently, the AGC threshold (RF level where the AGC starts to reduce the gain of the LNA) should be sufficiently high to reach a reasonable SNR above the threshold level. On the other hand, the threshold level should be set low enough to reduce the gain before the signal distortion exceeds an acceptable level.

Assuming a receiver sensitivity of -110 dBm for instance, a threshold in the RF range between -60 dBm and -70 dBm yields a sufficient high SNR when the AGC reduces the LNA gain. A sufficiently high SNR is achieved because the AGC starts to reduce the gain only when the RF input level is 40 to 50 dB or more above the sensitivity level. In addition, the distortion of the signal at -70 dBm to -60 dBm is relatively small, so the AGC will keep the distortion small over a certain range above the threshold level.

To set the threshold voltage to a value corresponding to a RF input level 40 dB to 50 dB above the sensitivity limit, an RF input signal has to be applied on the RF input (antenna) which is 40 dB to 50 dB higher than the sensitivity limit. Since the voltage on the Peak Detector output (PDO / pin 26) is equal to the RSSI voltage, applied on the non-inverting input of the OTA of the AGC, this voltage should be applied on pin 23 (THRES) to get a threshold voltage corresponding to a RF level 40 dB to 50 dB above the sensitivity limit. A voltage divider connected to the 3 V reference output at pin 24 can be calculated to provide the desired threshold voltage (V_{THRES}) at pin 23. The net sum of the resistor divider is recommended to be 600 k Ω .

4 AGC Inactive Mode

The inactive mode means that the LNA is forced either to high gain mode or to low gain mode independent of the RF signal level.

4.1 Low Gain Mode

The low gain mode is achieved by applying a voltage to pin 23 such that V_{THRES} is 0 to 0.7 V. This can easily be achieved by simply connecting pin 23 to ground. Pin 23 could be actively controlled as well by setting the port of a microcontroller low. In the low gain mode the dynamic range of the receiver can be extended and the risk of distortion due to an interferer could be reduced. This mode may be desired if an external LNA with a low Noise Figure (NF) is used on the front-end of the receiver to improve the sensitivity. Setting the LNA in the low gain mode should be considered if the gain of the external LNA is more than 12 dB because the overall CP1dB through the receiver frontend is decreased by the additional gain. Additionally, the high overall gain and poor PCB layout could comply with the condition for oscillation due to cross coupling between the output of the LNA (LNO) and the input of the external LNA. Consequently the external LNA input should not be placed close to the internal LNA output on the PCB. . Therefore, these RF frontend circuits should be arranged more in a row from antenna input to LNA input than in a circle. The capacitor at pin 4 is required also when forcing the LNA to low gain mode.

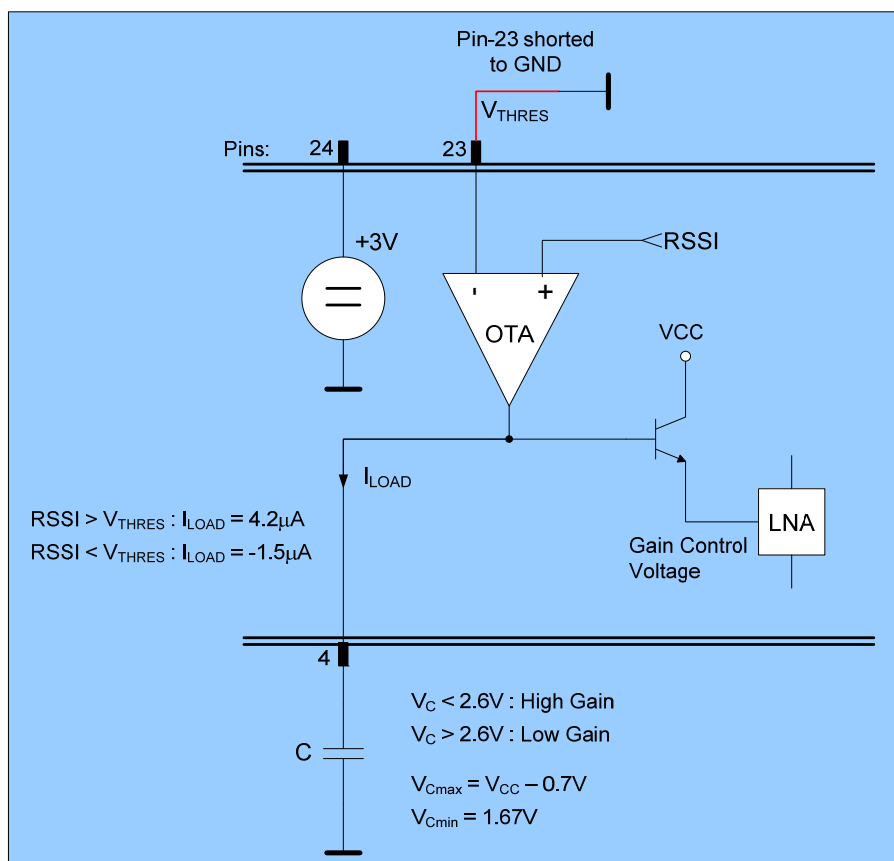


Figure 4 Forcing the LNA in the low gain mode

4.2 High Gain Mode

The LNA of all bipolar receivers (TDA520x, TDA521x, TDA522x, TDA7200, TDA7210 and TDA7210V) could be forced in high gain mode by applying a voltage of 3.3 V or higher on pin 23 (THRES). However, this pin 23 voltage must not be higher than $V_{CC} - 1$ V. Thus a DC-voltage between 3.3 V and $V_{CC} - 1$ V is required. Fortunately there is also another possibility to force the LNA into high gain mode. By connecting the 3 V reference voltage from pin 24 directly to pin 23 (V_{THRES}) and connecting pin 4 directly to ground (instead of using a capacitor to ground) the LNA will be forced into high gain mode. Please see Figure 5. Furthermore, in addition to this configuration being a cost saving by deleting a capacitor, it can also increase the ESD robustness at pin 4. Connecting pin 4 to ground will assure that the LNA will be in the high gain mode regardless of the amplitude of the RSSI voltage and consequently regardless of the RF input signal level. This configuration will work for all receivers called out in this application note.

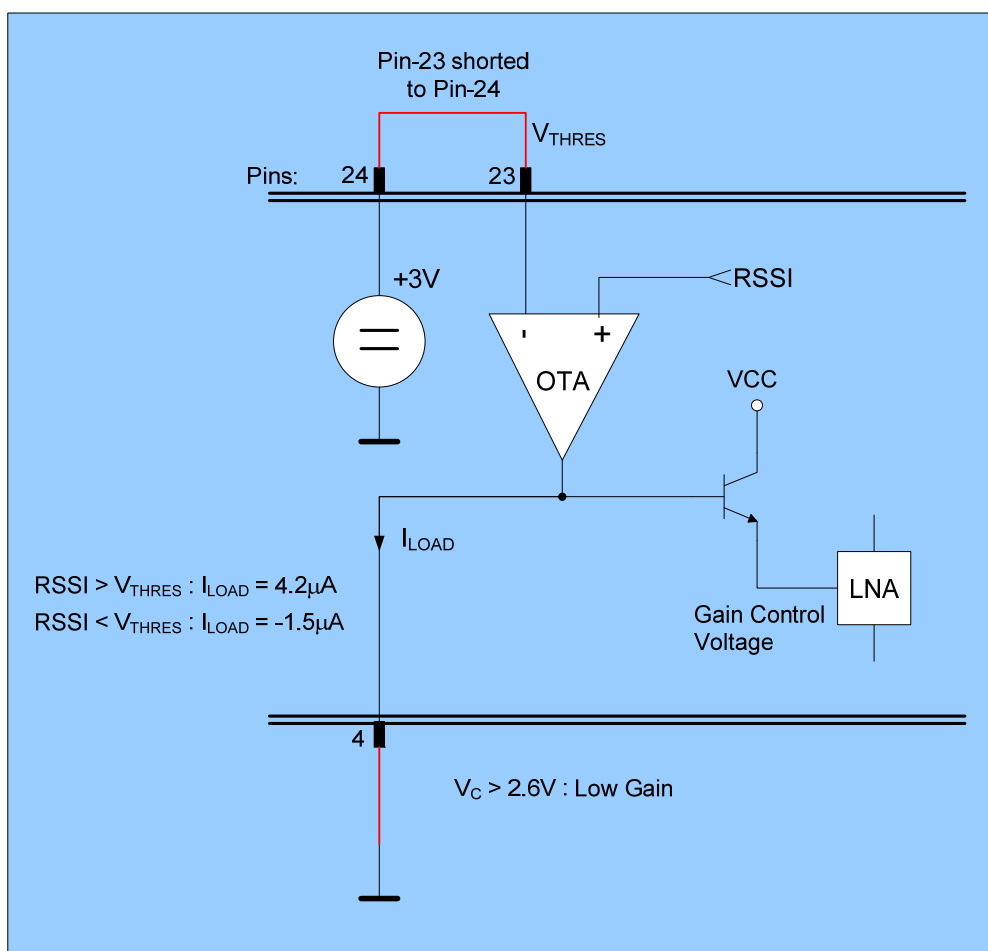


Figure 5 Forcing the LNA in the high gain mode with pin 4 grounded

5 RSSI Curves for Active and Inactive Modes

As already explained in chapter 3, the inactive mode means that the LNA is either forced to high gain mode or to low gain mode, regardless of the RF input level. In active mode, the threshold of the AGC is set to a voltage which is anywhere in between the RSSI voltage range. The range where the AGC is active means the RF input level range within the AGC is able to reduce the gain further with increasing RF input level, so the range within the AGC keeps the RSSI voltage almost constant. The RSSI curves in Figure 6 show the RSSI voltage over the RF input level and how the dynamic range of the receiver can be increased by using the AGC circuit in the active mode. When the LNA is forced to high gain mode, the AGC circuit is inactive over the whole RF input level range and the dynamic range of the receiver is consequently reduced by 20 dB. Incipient from above the noise floor up to saturation, the slope of the RSSI voltage is always the same, both in high gain mode and in low gain mode, except the range where the AGC is active.

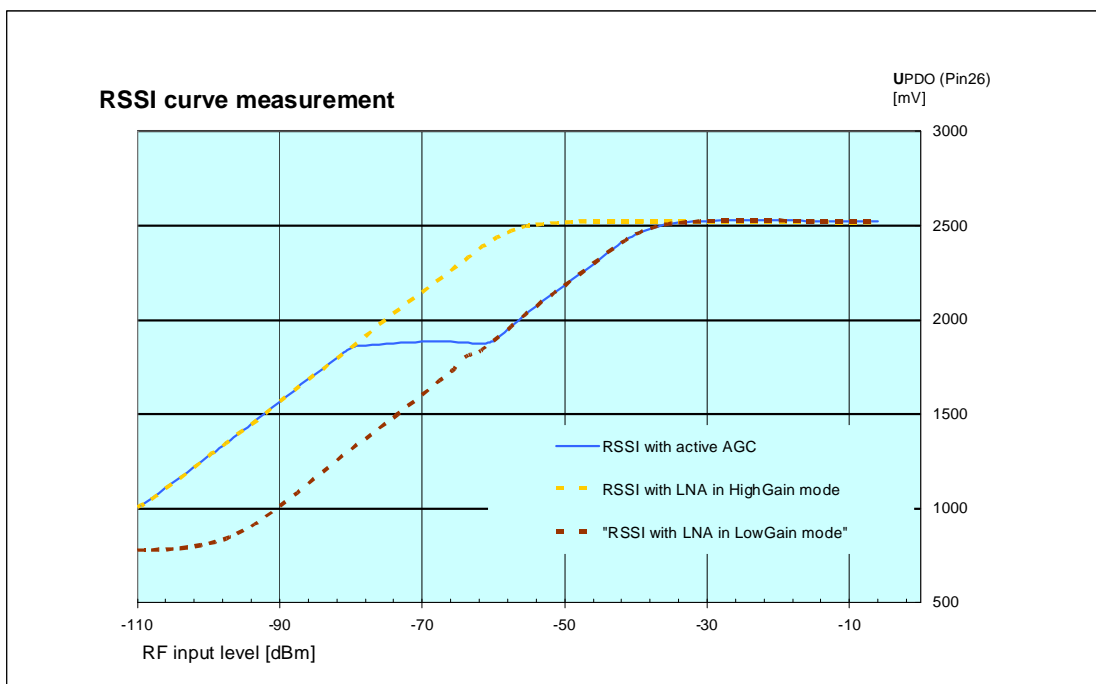


Figure 6 RSSI curves for active and inactive modes

6 Conclusion

To use the AGC circuit in the active mode, the threshold voltage (V_{THRES}) at pin 23 needs to be set such that when the AGC starts reducing the gain, the SNR is sufficiently large and significantly larger than at the sensitivity limit. Also the capacitor used at pin 4 should be set such that the time constant associated to the fast attack and slow decay is appropriate for the data rate of the receiver in the given application.

In the inactive mode, the LNA can be forced into the low gain mode by connecting pin 23 to ground, or applying a voltage to pin 23 that is at least lower than 0.7 V. The dynamic range of the receiver can be extended by ~20 dB by using the receiver in the active mode. Also by using a shunt resistor from pin 12 (IFO) to ground, the IIP3 of the LNA and mixer stages is increased by ~9 dB at 434 MHz for instance.

The LNA can alternatively be forced into the high gain mode by connecting pin 23 directly to pin 24 and pin 4 directly to GND. This would save a capacitor on pin 4 in addition.

In no case can pin 4 be left open in any of the active or inactive AGC modes of operation.

www.infineon.com