

Design guide for low-noise transistors in SDARS active antenna LNA

RF bipolar transistors

About this document

Scope and purpose

This application note provides application circuit design examples of Infineon's low-noise bipolar silicon (Si) and silicon germanium: carbon (SiGe:C) transistors for satellite digital audio radio service (SDARS) active antenna low noise amplifiers (LNAs). In this document, the transistor-based LNA schematics, printed circuit board (PCB) layouts and measurement results are shown. This document is relevant to the following low-noise transistor:

•	<u>BFP450</u>	SDARS LNA for 2320-2345 MHz
•	BFP640ESD	SDARS LNA for 2320-2345 MHz

- <u>BFP650</u> SDARS LNA for 2320-2345 MHz
- <u>BFP740F</u> SDARS LNA for 2320-2345 MHz

Intended audience

This document is intended for engineers who need to design active antenna LNA for SDARS applications.

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1 Introduction

1.1 SDARS active antenna LNA

SDARS is a digitally encoded satellite radio. The signals are broadcasted from satellites to earth-based receivers directly or via repeater stations operating in the S-band from 2320–2332.5 MHz and 2332.5–2345 MHz. SDARS provides paying subscribers with over 175 channels of "MP3-quality" digital radio wherever they are, in their vehicle or at home.

An SDARS system utilizes dual transmitter broadcasting formats which comprise the simultaneous transmission of signals from both satellites and terrestrial transmitters. The satellite transmissions cover by far most of the geographic broadcast area. The terrestrial transmissions supplement the satellite coverage primarily in urban regions where the satellite signals may be obstructed by tall buildings and structures. An SDARS active antenna is necessary to provide good reception for both terrestrial and satellite signals. The active part of an SDARS active antenna is a cascaded chain of LNAs to achieve both the low noise figure and the high gain while maintaining high linearity. A general topology for the SDARS active antenna is shown in Figure 1. This application note presents Infineon low noise transistors which can be used for active antenna LNA in the SDARS receiver.



Figure 1 Block diagram example of the SDARS active antenna



Introduction

1.2 Infineon RF transistor family

Infineon Technologies provides high-performance Radio-Frequency (RF) transistors targeting SDARS applications. Infineon's reliable high-volume RF transistors offer exceptionally low noise figure, high gain, and high linearity at low power consumption levels for RF applications. The fourth-generation transistor is based on bipolar Si technologies, and the sixth- and seventh-generation are based on robust ultra low-noise SiGe: C technologies. Their optimized inner transistor cell structures lead to best-in-class power gain and NF at SDARS operating frequency. The transistors maximize the design flexibility to customer requirements.



2 Application circuits and performance overview

2.1 SDARS active antenna 1st stage LNA

The LNA described in this section can be used for the active antenna 1st stage LNA in the SDARS receiver providing very low NF, higher gain, and high linearity.

2.1.1 **Performance overview**

The following table shows the performance of the SDARS LNA with RF low noise bipolar transistor <u>BFP740F</u>.

Parameter	Symbol		Value			Notes
Device			<u>BFP740F</u>			
Bias voltage	V _{cc}		3.3		V	
Bias current	I _{cc}		12.9		mA	
Frequency	f	2320	2332.5	2345	MHz	
Gain	G	18.3	18.2	18.2	dB	
Noise figure	NF	0.71	0.7	0.68	dB	
Input return loss	RL _{in}	10.2	10.3	10.3	dB	
Output return loss	RL _{out}	11	10.9	10.8	dB	
Reverse isolation	ISO _{rev}	28	27.9	27.9	dB	
Output 1-dB compression point	OP _{1dB}		5.6		dBm	Measured at 2332.5 MHz
Output third- order intercept point	OIP ₃	22.95			dBm	$P_{IN} = -25 \text{ dBm per tone}$ $f_1 = 2331 \text{ MHz}$ $f_2 = 2332 \text{ MHz}$
Stability	К		>1			Measured from 15 MHz to 13 GHz

 Table 1
 Summary of measurement results for SDARS active antenna 1st stage LNA with <u>BFP740F</u>

2.1.2 Schematic

The following figure presents the schematic of the SDARS active antenna 1st stage LNA with <u>BFP740F</u>. Emitter degeneration provides negative feedback to achieve the transistor impedance matching and low-noise matching at the same time. In the LNA circuit, resistors R1 and R2 stand for transistor voltage and current bias, meanwhile, they form a negative DC feedback mechanism to stabilize the transistor bias points in various conditions. Capacitors C2 and C3 serve as the RF bypass. The transistor input matching can be achieved by the capacitor C1 and the inductor L1. The output matching network is formed by L2, C4, C5, R3, and R4. Resistors R3 and R4 also support the improvement of circuit stability.



Application circuits and performance overview





2.1.3 Bill of Materials (BOM)

Symbol	Value	Unit	Package	Manufacturer	Notes
Q1	<u>BFP740F</u>		TSFP-4	Infineon	SiGe: C low-noise transistor
C1	22	рF	0402	Various	Input matching and DC blocking
C2	220	nF	0402	Various	RF decoupling
C3	220	nF	0402	Various	RF decoupling
C4	3.3	pF	0402	Various	Output matching and stability improvement
C5	1.5	pF	0402	Various	Output matching and DC blocking
R1	30	Ω	0402	Various	DC biasing
R2	47	kΩ	0402	Various	Base DC biasing
R3	30	Ω	0402	Various	Low-frequency stability improvement
R4	240	Ω	0402	Various	Output matching and stability improvement
L1	10	nH	0402	Murata LQG	Input matching
L2	4.7	nH	0402	Murata LQG	Output matching

Table 2 BOM of the SDARS active antenna 1st stage LNA with <u>BFP740F</u> transistor



2.1.4 Evaluation board and PCB layout information

The evaluation board for the SDARS active antenna 1st stage LNA with <u>BFP740F</u> transistor:

- PCB material: FR4
- PCB marking: M100511

The photo of the evaluation board for the SDARS active antenna 1st stage LNA with <u>BFP740F</u> and the detailed description of the PCB stack are shown in the following figures.



Figure 3 Photo of the evaluation board with PCB marking M100511 (left) and emitter degeneration details (right)



Figure 4 PCB stack information for the evaluation board with PCB marking M100511



2.1.5 Measurement results of the SDARS active antenna 1st stage LNA¹⁾



Figure 5Small signal gain of the SDARS active antenna 1st stage LNA with BFP740F transistor



Figure 6Small signal gain of the SDARS active antenna 1st stage LNA with BFP740F transistor (detail view)

Note: 1) The graphs are generated with the AWR electronic design automation (EDA) software Microwave Office®.

Application circuits and performance overview



Figure 7 Input return loss measurement of the SDARS active antenna 1st stage LNA with <u>BFP740F</u> transistor



transistor







Figure 9Reverse isolation measurement of the SDARS active antenna 1st stage LNA with BFP740F
transistor



transistor

infineon

Application circuits and performance overview



Figure 11Input 1-dB compression point measurement of SDARS active antenna 1st stage LNA withBFP740F transistor



 Figure 12
 3rd order Intermodulation distortion measurement of SDARS active antenna 1st stage LNA with BFP740F

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Figure 13 Stability K factor plot of the SDARS active antenna 1st stage LNA with <u>BFP740F</u> transistor





2.2 SDARS active antenna 2nd stage LNA

The LNA described in this section can be used for the active antenna 2nd stage LNA in the SDARS receiver which provides low NF and high linearity.

2.2.1 Performance overview

The following table shows the performance of the SDARS 2nd stage LNA with RF low-noise bipolar transistor <u>BFP640ESD</u>.

Parameter	arameter Symbol Value			Unit	Notes	
Device			BFP640ESD			
Bias voltage	V _{cc}		3.3		V	
Bias current	I _{cc}		23.6		mA	
Frequency	f	2320	2332.5	2345	MHz	
Gain	G	18.8	18.7	18.7	dB	
Noise figure	NF	1.0	1.0	1.0	dB	
Input return loss	RL _{in}	11.8	11.9	12.1	dB	
Output return loss	RL_{out}	16.8	16.4	16	dB	
Reverse isolation	ISO _{rev}	23.6	23.6	23.5	dB	
Output 1-dB compression point	OP_{1dB}		13.4		dBm	Measured at 2332.5 MHz
Output third- order intercept point	OIP ₃	30.1			dBm	$P_{IN} = -20 \text{ dBm per tone}$ $f_1 = 2332 \text{ MHz}$ $f_2 = 2333 \text{ MHz}$
Stability	К	< >11				Measured from 100 MHz to 13 GHz

 Table 3
 Summary of measurement results for the SDARS 2nd stage LNA with <u>BFP640ESD</u>

2.2.2 Schematic

The following figure presents the schematic of the SDARS active antenna 2nd stage LNA with <u>BFP640ESD</u>. Emitter degeneration provides negative feedback to achieve the transistor impedance matching and low-noise matching at the same time. In the LNA circuit, resistors R1 and R3 stand for transistor voltage and current bias, meanwhile, they form a negative DC feedback mechanism to stabilize the transistor bias points in various conditions. Capacitors C2, C3, and C4 serve as RF bypass. The transistor input matching can be achieved by the capacitor C1 and the inductor L1. The output matching network is formed by L2, C5, C6, and R3. Resistor R3 also supports the improvement of circuit stability.







2.2.3 Bill of Materials (BOM)

Symbol	Value	Unit	Package	Manufacturer	Notes
Q1	BFP640ESD		SOT343	Infineon	SiGe: C low noise transistor
C1	8.2	рF	0402	Various	Input matching and DC blocking
C2	8.2	pF	0402	Various	RF Decoupling
C3	220	nF	0402	Various	RF decoupling
C4	220	nF	0402	Various	RF decoupling
C5	8.2	рF	0402	Various	Output matching and stability improvement
C6	1.5	pF	0402	Various	Output matching and DC blocking
R1	9.1	Ω	0402	Various	DC biasing
R2	20	kΩ	0402	Various	Base DC biasing
R3	2.2	Ω	0402	Various	Low-frequency stability improvement
L1	15	nH	0402	Murata LQG	Input matching
L2	3.0	nH	0402	Murata LQG	Output matching

Table 4 BOM of the SDARS active antenna 2nd stage LNA with <u>BFP640ESD</u> transistor



2.2.4 Evaluation board and PCB layout information

The evaluation board for the SDARS active antenna 2nd stage LNA with <u>BFP640ESD</u> transistor:

- PCB material: FR4
- PCB marking: M11118

The photo of the evaluation board for the SDARS active antenna 2nd stage LNA with <u>BFP640ESD</u> and the detailed description of the PCB stack are shown in the following figures.



Figure 15 Photo of evaluation board with the PCB marking M11118 (left) and emitter degeneration details (right)



Figure 16 PCB stack information for the evaluation board with the PCB marking M11118



2.2.5 Measurement results of the SDARS active antenna 2nd stage LNA with BFP640ESD transistor¹⁾



Figure 17 Small signal gain of the SDARS active antenna 2nd stage LNA with <u>BFP640ESD</u> transistor



Figure 18Small signal gain of the SDARS active antenna 2nd stage LNA with BFP640ESD transistor(detail view)

Note: 1) The graphs are generated with the AWR EDA software Microwave Office[®].



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Figure 19Input return loss measurement of the SDARS active antenna 2nd stage LNA with BFP640ESD
transistor



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Figure 21Reverse isolation measurement of the SDARS active antenna 2nd stage LNA withBFP640ESDtransistor



transistor

neon

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Figure 23Input 1-dB compression point measurement of the SDARS active antenna 2nd stage LNAwith BFP640ESD transistor



Figure 243rd order Intermodulation distortion measurement of the SDARS active antenna 2nd stageLNA with BFP640ESD

Infineon





2.5

5100

Frequency (MHz)

Stability K factor plot of the SDARS active antenna 2nd stage LNA with <u>BFP640ESD</u>

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RF bipolar transistors

3

2

1.5

1

0.5

0

100

transistor

K Factor

Figure 25

7505.8 MHz 1.001

BFP640ESD LNA

13000

10100





2.3 SDARS active antenna 3rd stage LNA

The LNA described in this section can be used for the active antenna 3rd stage LNA in the SDARS receiver which provides very high linearity.

2.3.1 Performance overview

The following table shows the performance of the SDARS active antenna 3rd stage LNA with RF low-noise bipolar transistor <u>BFP450</u> or <u>BFP650</u>.

Table 5	Summary of measurement results for the SDARS active antenna 3 rd stage LNA with <u>BFP450</u> or
	<u>BFP650</u>

Parameter	Symbol		Value					Unit	Notes
Device			<u>BFP450</u>			<u>BFP650</u>			
Bias voltage	V _{cc}		3.3			3.3		V	
Bias current	I _{cc}		88.2		57.2			mA	
Frequency	f	2320	2332.5	2345	2320	2332.5	2345	MHz	
Gain	G	10.3	10.3	10.3	14.3	14.2	14.2	dB	
Noise figure	NF	2.6	2.6	2.6	1.2	1.2	1.2	dB	
Input return loss	RL _{in}	10.4	10.7	11.1	14.8	14.6	14.4	dB	
Output return loss	RL _{out}	16	16.2	16.3	12.3	12	11.7	dB	
Reverse isolation	ISO _{rev}	16.4	16.4	16.3	18.3	18.3	18.3	dB	
Output 1-dB compression point	OP _{1dB}	17.81			17.37		dBm	Measured at 2332.5 MHz	
Output third- order intercept point	OIP ₃	32.78			30.2		dBm	P _{IN} = -10 dBm per tone f ₁ = 2332 MHz f₂ = 2333 MHz	
Stability	к		>1			>1			Measured from 100 MHz to 13 GHz

2.3.2 Schematic

The following figure presents the schematic of the SDARS active antenna 2nd stage LNA with <u>BFP450</u> or <u>BFP650</u>. Emitter degeneration provides negative feedback to achieve the transistor impedance matching and low noise matching at the same time. In the LNA circuit, resistors R1 and R2 stand for transistor voltage and current bias, meanwhile, they form a negative DC feedback mechanism to stabilize the transistor bias points in various conditions. Capacitors C3, C4, and C5 serve as RF bypass. The transistor input matching can be achieved by C1, C2, C8, and L1. The output matching network is formed by C6, C7, R3, and L2. Resistor R3 also supports the improvement of circuit stability.







2.3.3 Bill of Materials (BOM)

Table 0 DOM OF the SDARS active antenna 5 stage Lives with $\frac{DFF+30}{DFF+30}$ of $\frac{DFF+30}{DFF+30}$ transistor							
Va	lue	Unit	Package	Manufacturer	Notes		
			COTOAO	Infinoon	BFP450-Si bipolar transistor and		
<u>DFP430</u>	<u>DFP030</u>		501343	mmeon	BFP650-SiGe: C low-noise transistor		
1	n.c.	рF	0402	Various	Input matching and DC blocking		
2.7		рF	0402	Various	Input matching and DC blocking		
8.2	8.2	рF	0402	Various	RF Decoupling		
220	220	nF	0402	Various	RF decoupling		
220	220	nF	0402	Various	RF decoupling		
8.2	0.2	۲	0402	Various	Output matching		
	ð.Z	рг			and stability improvement		
2.2	2.2	рF	0402	Various	Output matching and DC blocking		
n.c. ¹⁾	1	рF	0402	Various	Input matching and DC blocking		
4.3	5.1	Ω	0402	Various	DC biasing		
1.5	4.7	kΩ	0402	Various	Base DC biasing		
2.2	4.7	Ω	0402	Various	Low-frequency stability improvement		
12	12	nH	0402	Murata LQG	Input matching		
5.1	5.1	nH	0402	Murata LQG	Output matching		
	Va BFP450 1 2.7 8.2 220 8.2 220 8.2 2.2 n.c. ¹⁾ 4.3 1.5 2.2 12 5.1	Value BFP450 BFP650 1 n.c. 2.7 8.2 8.2 8.2 220 220 220 220 8.2 8.2 2.2 2.2 n.c. ¹⁾ 1 4.3 5.1 1.5 4.7 2.2 4.7 12 12 5.1 5.1	Value Unit BFP450 BFP650 1 n.c. pF 2.7 pF 8.2 8.2 pF 220 220 nF 220 220 nF 8.2 8.2 pF 2.2 2.2 pF n.c. ¹⁾ 1 pF 4.3 5.1 Ω 1.5 4.7 kΩ 2.2 4.7 Ω 12 12 nH 5.1 5.1 nH	ValueUnitPackageBFP450BFP650SOT3431n.c.pF04022.7pF04028.28.2pF0402220220nF0402220220nF04028.28.2pF0402220220nF0402220220nF04028.28.2pF04021.54.7Ω04021.54.7Ω04021.212nH04025.15.1nH0402	ValueUnitPackageManufacturerBFP450BFP650SOT343Infineon1n.c.pF0402Various2.7pF0402Various8.28.2pF0402Various220220nF0402Various220220nF0402Various8.28.2pF0402Various220220nF0402Various8.28.2pF0402Various8.23.2pF0402Various1pF0402Various1.54.7Ω0402Various1.54.7Ω0402Various1.212nH0402Murata LQG5.15.1nH0402Murata LQG		

Table 6	BOM of the SDARS active antenna 3 rd stage LNAs with <u>BFP450</u> or <u>BFP650</u> transistor
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Note: 1) Not connected (n.c.).



2.3.4 Evaluation boards and PCB layout information

The evaluation board for the SDARS active antenna 3rd stage LNA with <u>BFP450</u> and <u>BFP650</u> transistor:

- PCB material: FR4
- PCB marking: M11118

The photo of the evaluation board for the SDARS active antenna 3rd stage LNA with <u>BFP450</u> or <u>BFP650</u> and the detailed description of the PCB stack are shown in the following figures.



Figure 27 Photo of the evaluation board with the PCB marking M11118 (left) and emitter degeneration details (right)



Figure 28 PCB stack information for the evaluation board with the PCB marking M11118



2.3.5 Measurement results of the SDARS active antenna 3rd stage LNA with <u>BFP450</u> or <u>BFP650</u> transistor¹⁾



Figure 29 Small signal gain of the SDARS active antenna 3rd stage LNA with <u>BFP450</u> or <u>BFP650</u> transistor



Figure 30Small signal gain of the SDARS active antenna 3rd stage LNA with <a href="https://www.berefattingenergy-base-stage-likeling-stage-likelin

Note: 1) The graphs are generated with the AWR EDA software Microwave Office®.

Application circuits and performance overview



Figure 31 Input return loss measurement of the SDARS active antenna 3rd stage LNA with <u>BFP450</u> or <u>BFP650</u> transistor







Application circuits and performance overview



Figure 33Reverse isolation measurement of the SDARS active antenna 3rd stage LNA with BFP450 orBFP650transistor



Figure 34 Noise figure measurement of the SDARS active antenna 3rd stage LNA with <u>BFP450</u> or <u>BFP650</u> transistor



2331.5

2332 MHz

-0.09



2333 MHz -0.07



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Figure 35Input 1-dB compression point measurement of the SDARS active antenna 3rd stage LNAwith BFP650 transistor

10

-10

-90

2330.5

2332.5

Frequency (MHz)

2333.5

2334.5

BFP450 LNA



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Application circuits and performance overview



Figure 373rd order Intermodulation distortion measurement of the SDARS active antenna 3rd stageLNA with BFP650



Frequency (MHz)

5100

- BFP450 LNA --- BFP650 LNA

10100

4

0

100

13000



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Revision history

Revision history

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