

### XMC1000

### **About this document**

### **Scope and purpose**

This document presents a method and algorithm that automatically adjusts the LED current ripple in a Continuous Conduction Mode (CCM) Buck LED driver solution with an XMC1000 microcontroller according to changes in supply voltage and LED forward voltage, to maintain average LED current.

#### **Intended audience**

This document is intended for engineers who wish to implement LED lighting applications with the XMC1000 microcontroller.

### **Applicable Products**

- XMC120x
- XMC130x
- XMC140x
- DAVE™

#### References

Infineon: DAVE™, <a href="http://www.infineon.com/DAVE">http://www.infineon.com/DAVE</a>

Infineon: XMC<sup>™</sup> Family, <a href="http://www.infineon.com/XMC">http://www.infineon.com/XMC</a>

Infineon: AN\_201609\_PL30\_028 - Driving LEDs with XMC1000, <a href="http://www.infineon.com/XMC1000">http://www.infineon.com/XMC1000</a>

Infineon: XMC<sup>™</sup> LED Current Control Explorer Kit, <a href="http://www.infineon.com/xmc">http://www.infineon.com/xmc</a> led cc exp



Introduction

### **Table of contents**

About t	this document	
Table o	of contents	
	Introduction	
2	Method	5
3		
4	Hardware	g
4.1	Altering the target average LED current	10
5	Software	11
Revision history		13



Introduction

### 1 Introduction

Continuous Conduction Mode (CCM) Buck is a popular method of secondary-side LED driving because of its efficiency. A feature of the CCM buck method is the LED current ripple, which is an effect of the controller turning the MOSFET on and off in order to get a stable average current at a required value (Figure 1).

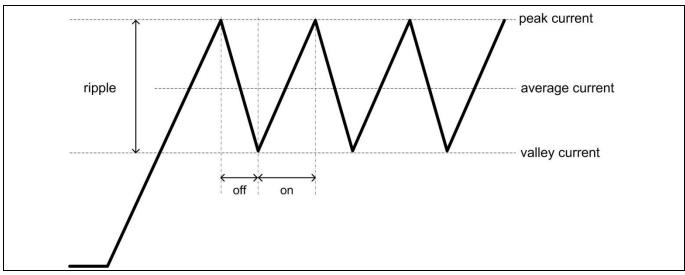


Figure 1 LED current ripple

One implementation method is to use two comparators to detect the peak and valley current respectively. The low-cost solution with XMC1000 microcontrollers uses an inverted buck configuration and implements a 'single-comparator-based peak-current detection with fixed off time' control of the LED current (Figure 2) per LED string. This means that the comparator detects the peak current level, then MOSFET is turned off for a predetermined period of time. This is defined as 'off time', and it determines the ripple size and therefore the average current value.

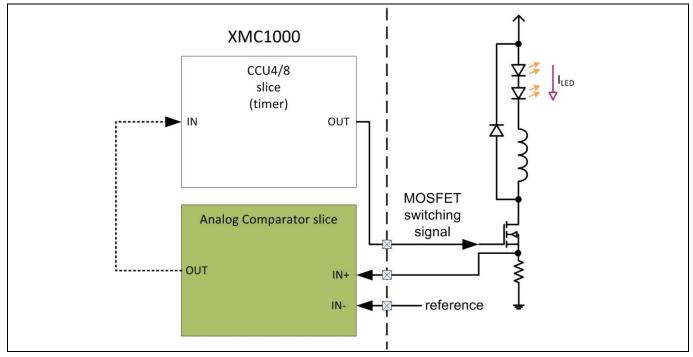


Figure 2 Single-comparator-based peak-current control circuitry



#### Introduction

With a couple of measurements and a software algorithm, a method can be devised to re-calculate the required 'off time' in order to maintain the average LED current regardless of changes to the LED supply voltage and LED forward voltage. We explain the details of this method in this document.

Note:

More information on the 'peak-current detection with fixed off time' control can be found in the application note AN\_201609\_PL30\_028.



Method

### 2 Method

In addition to the microcontroller resources required to implement the CCM Buck LED driver (as documented in AN\_201609\_PL30\_028), two Analog-to-Digital Converter (ADC) channels are required; one to measure the input voltage ( $V_{in}$ ) and the other to measure the inductance voltage ( $V_{in}$ ) on the channel (Figure 3). Any additional LED channels will require an additional ADC channel to measure the channel's  $V_{in}$ . The XMC130x microcontrollers can drive up to 3 LED channels, and the XMC140x variants can drive up to 4 LED channels.

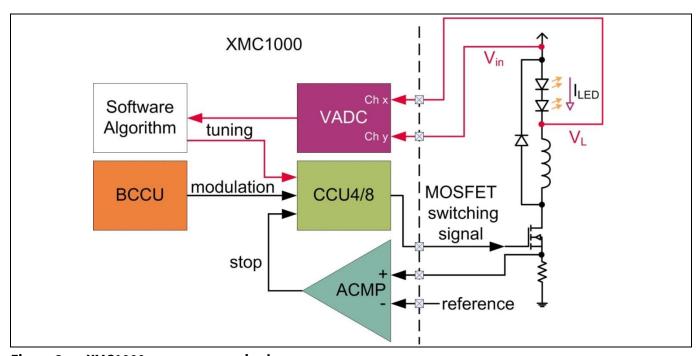


Figure 3 XMC1000 resources required

Figure 4 shows the LED current ripple and introduces the parameters involved in the ripple tuning process.

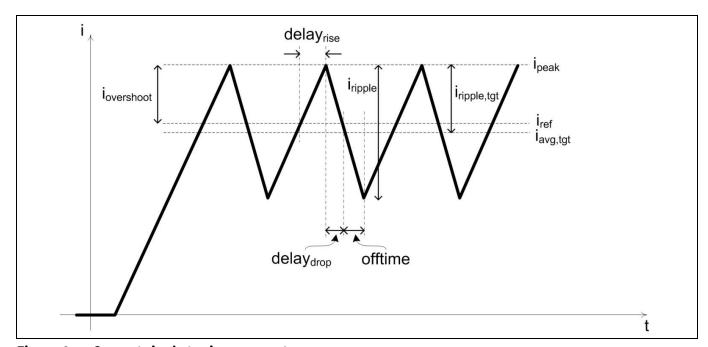


Figure 4 Current ripple tuning parameters

# infineon

#### Method

The reference value (i<sub>ref</sub>) for the peak current level can be set either by an external resistive divider or a pseudo Digital-to-Analog Converter (DAC). The instantaneous LED current will over-shoot the peak reference value slightly (Figure 4), due to internal signal propagation delay in the XMC1000 microcontroller. The amount of over-shoot depends on the propagation delay and the steepness of the LED current rise slope.

The propagation delay is typically a fixed value given for the device and routing option selected. The steepness of the LED current rises slope or how fast the LED current rises depends on  $V_{in}$ , LED forward voltage ( $V_F$ ), and the inductance (L). Typically the inductance is also a fixed value.

Ignoring voltage drops over the diode, shunt resistor, and MOSFET during on-time, the LED current rise slope can be described by the following equation:

$$\frac{\delta i}{\delta t} = \frac{V_{in} - V_F}{L}$$
$$= \frac{V_L}{L}$$

The amount of LED current overshoot is therefore derived as:

$$i_{overshoot} = \frac{\delta i}{\delta t} \times delay_{rise}$$
  
=  $\frac{V_L}{I} \times delay_{rise}$ 

The peak LED current value can then be calculated:

$$i_{peak} = i_{ref} + i_{overshoot}$$

The LED current ripple depends on the period of time the MOSFET is turned off and the steepness of the LED current drop slope. The MOSFET off-time is contributed by a small propagation delay (delay<sub>drop</sub>) and the configured off-time or COMPARE value for the CCU4/8 time slice.

The LED current drop slope can be described as:

$$\frac{\delta i}{\delta t} = \frac{V_F}{L}$$
$$= \frac{V_{in} - V_L}{L}$$

The LED current ripple can then be measured as:

$$i_{ripple} = \frac{\delta i}{\delta t} \times (delay_{drop} + offtime)$$
  
=  $\frac{V_{in} - V_L}{L} \times (delay_{drop} + offtime)$ 

For this automatic current ripple tuning method, the target average LED current value that is to be maintained by the CCM buck LED driver is defined as a value 5% lower than  $i_{ref}$ :

$$i_{avg,tgt} = \frac{i_{ref}}{105} \times 100$$

The half-ripple value is defined as:

$$i_{rinnle,tat} = i_{neak} - i_{ava,tat}$$



### Method

To achieve a stable  $i_{avg,tgt}$  value, the LED current is expected to drop by a total amount of (2 x  $i_{ripple,tgt}$ ) when the MOSFET is turned off.

The required CCU4/8 off-time can be calculated as:

$$\begin{split} off time &= \frac{L \times 2 \times i_{ripple,tgt}}{V_F} - delay_{drop} \\ &= \frac{L \times 2 \times i_{ripple,tgt}}{V_{in} - V_L} - delay_{drop} \end{split}$$



**Algorithm** 

### 3 Algorithm

The algorithm can be described with the following steps:

- 1. Measure  $i_{\text{ref}}$  if external resistive divider is used for the ACMP reference.
- 2. Calculate i<sub>avg,tgt</sub>.
- 3. Measure V<sub>in</sub>.
- 4. Start MOSFET switching with large ripple configuration.
- 5. Measure V<sub>L</sub>.
- 6. Calculate V<sub>F</sub>.
- 7. Calculate i<sub>overshoot</sub>.
- 8. Calculate i<sub>ripple,tgt</sub>.
- 9. Calculate the required off-time.
- 10. Update CCU4/8 COMPARE value.
- 11. Monitor V<sub>in</sub> and V<sub>F</sub>. Repeat tuning process if significant change is observed.

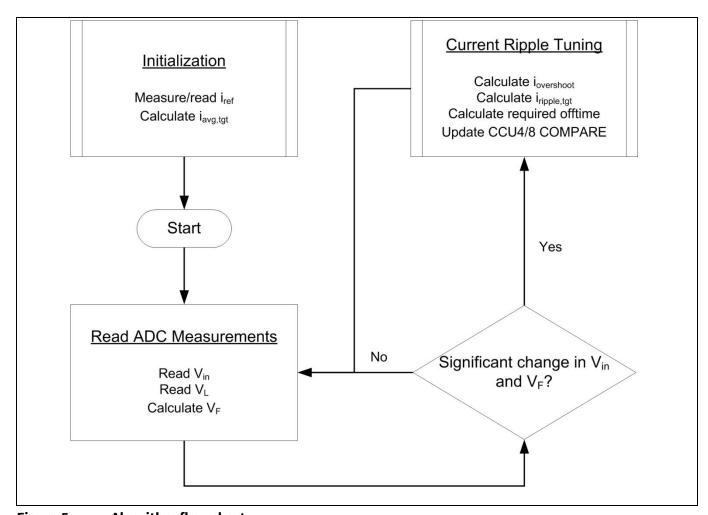


Figure 5 Algorithm flow chart



**Hardware** 

### 4 Hardware

The XMC™ LED Current Control Explorer (Figure 6) is an Infineon application kit that supports the automatic LED current ripple tuning method and algorithm.

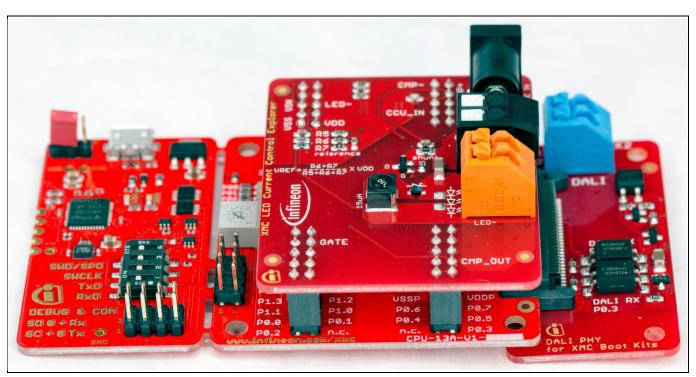


Figure 6 XMC™ LED Current Control Explorer

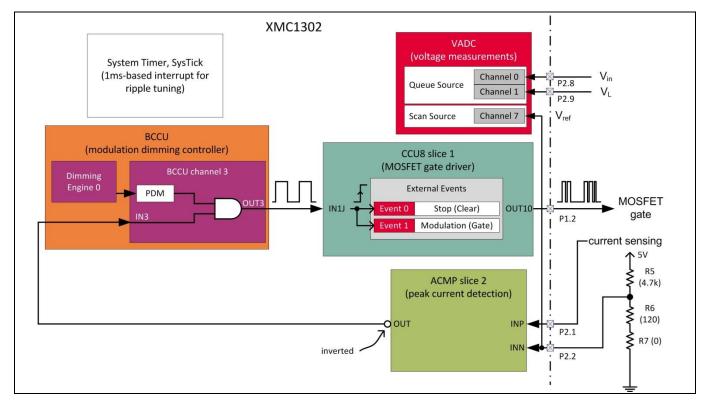


Figure 7 Hardware resources utilized in the XMC™ LED Current Control Explorer kit



**Hardware** 

### 4.1 Altering the target average LED current

The kit uses an external resistive divider circuit to generate a reference level for peak current detection. The reference level can be easily altered by using different combinations of  $R_6$  and  $R_7$  resistor values. To assist in the calculations of the required resistor values, an excel workbook titled "Automatic\_Current\_Ripple\_Tuning" is provided. In the sheet "Setup Hardware" (Figure 8), you are able to obtain the required  $R_6$  and  $R_7$  values for the required target average LED current.

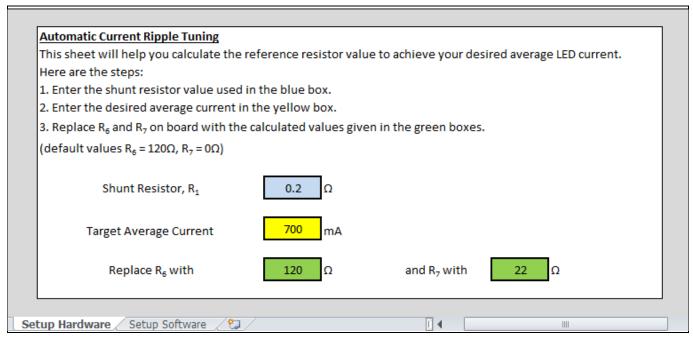


Figure 8 Resistor calculation help sheet

The excel workbook can be downloaded from the same <u>webpage link</u> as this document (Figure 9). Both files can be found in the 'Documents' tab (left-hand side of webpage) and under the 'Application Note' section (scroll down the webpage).

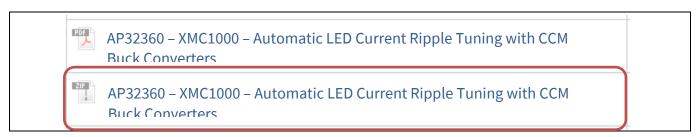


Figure 9 <u>Download link</u> for the excel workbook help-sheet



**Software** 

### 5 Software

The XMC<sup>™</sup> LED Current Control Explorer Kit comes with a project titled "LED\_CCEXP\_C2\_AUTOMATIC\_RIPPLE\_TUNING" which includes the automatic current ripple tuning feature. The project is developed based on DAVE<sup>™</sup> APPs in Infineon's free Integrated Development Environment (IDE) DAVE<sup>™</sup>. This project can be downloaded from the kit's official webpage.

In the project's main.c file, there is a MACROS section (Figure 10). The values defined have been pre-calculated based on the inductor and shunt resistor values. The scaling factors were selected to avoid overflow cases in the calculation steps.

```
main.c 🛭
  /* Macros for Automatic Current Ripple Tuning */
58 #define R SHUNT
                                                       /* (1/0.2) Ohm */
                                                      /* fixed propagation delay when turning off MOSFETs */
59 #define DELAY_DROP
                                              140U
                                              136533U /* IREF_SCALE_ADJUSTMENT/R_SHUNT/VREF_GAIN*(2^IREF_CALCULATION_SCALING) */
60 #define IREF_CALCULATION_CONSTANT
61 #define IREF CALCULATION SCALING
                                              15U
                                              124830U /* 100/105*(2^IAVG_CALCULATION_SCALING) */
62 #define IAVG_CALCULATION_CONSTANT
63 #define IAVG CALCULATION SCALING
                                              17U
                                                       /* DELAY RISE/L*IOVERSHOOT_SCALE_ADJUSTMENT */
64 #define IOVERSHOOT_CALCULATION_CONSTANT
                                              1U
65 #define OFFTIME_CALCULATION_CONSTANT
                                                       /* 2*L*OFFTIME SCALE ADJUSTMENT
                                              300U
   #define TIMER_COMPARE_CALCULATION_CONSTANT 16777U /* (1/TIMER_RESOLUTION)*(2^TIMER_COMPARE_CALCULATION_SCALING) */
   #define TIMER_COMPARE_CALCULATION SCALING
                                              18U
```

Figure 10 Definition of macros used in the calculations for ripple tuning

The excel workbook "Automatic\_Current\_Ripple\_Tuning" also comes with a worksheet titled "Setup Software" which provides an insight into the calculations of the values used. It also provides the equations described in 2 Method and their actual implementation forms in the code. This help sheet is also useful if you wish to experiment with different inductor and shunt resistor values. It allows you to enter the new values and the respective macro values will be automatically calculated, ready to be copied into the project (Figure 11).

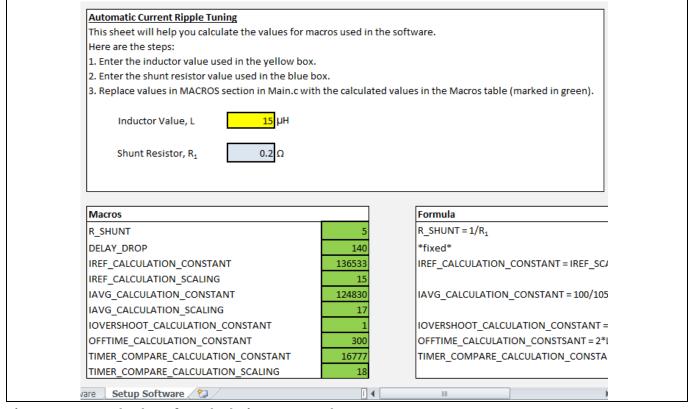


Figure 11 Help sheet for calculating macro values



#### **Software**

Two instances of ADC\_MEASUREMENT\_ADV APPs are used in the project:

- one to implement the ADC scan source for measuring V<sub>ref.</sub>
- one to implement the ADC queue source for measuring V<sub>in</sub> and V<sub>L</sub>.

The ADC scan source is configured as a one-shot conversion via a software trigger. This trigger is invoked at the start of the program right after the initialization of the peripherals. The result of the conversion is read in the callback function, void adc scan callback (void).

The conversions on the ADC queue source are triggered by the Pulse-Density Modulation (PDM) output of the Brightness and Color Control Unit (BCCU) channel. The results of the conversions are read in the callback function, void adc queue callback (void). In this callback function the results are checked for significant changes to trigger the current ripple tuning process.

Using the SYSTIMER APP, a software periodic timer with a 1ms-base is created. An interrupt is generated at the end of this timer period, with the tasks defined in the callback function, void mytimerinterrupt (void). Among the tasks carried out in this callback function is the LED current ripple tuning when required feature. The calculations for this task can be found in the function void current ripple tuning (void).



**Revision history** 

### **Revision history**

### Major changes since the last revision

Page or Reference	Description of change
All pages.	First release.

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