

# TLE5011

GMR-Based Angular Sensor

## Application Note TLE5011 Calibration

V 1.1

Sensors



Never stop thinking

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## 1 Giant Magneto-Resistance Parameters

The output signals of the TLE5011 can be factored into a sine (Y) and a cosine (X). These signals can be expressed by [Equation \(1\)](#).

$$\begin{aligned} X &= A_X * \cos(\alpha + \varphi_X) + O_X \\ Y &= A_Y * \sin(\alpha + \varphi_Y) + O_Y \end{aligned} \quad (1)$$

$A_X$  .. Amplitude of X(COS) signal

$A_Y$  .. Amplitude of Y(SIN) signal

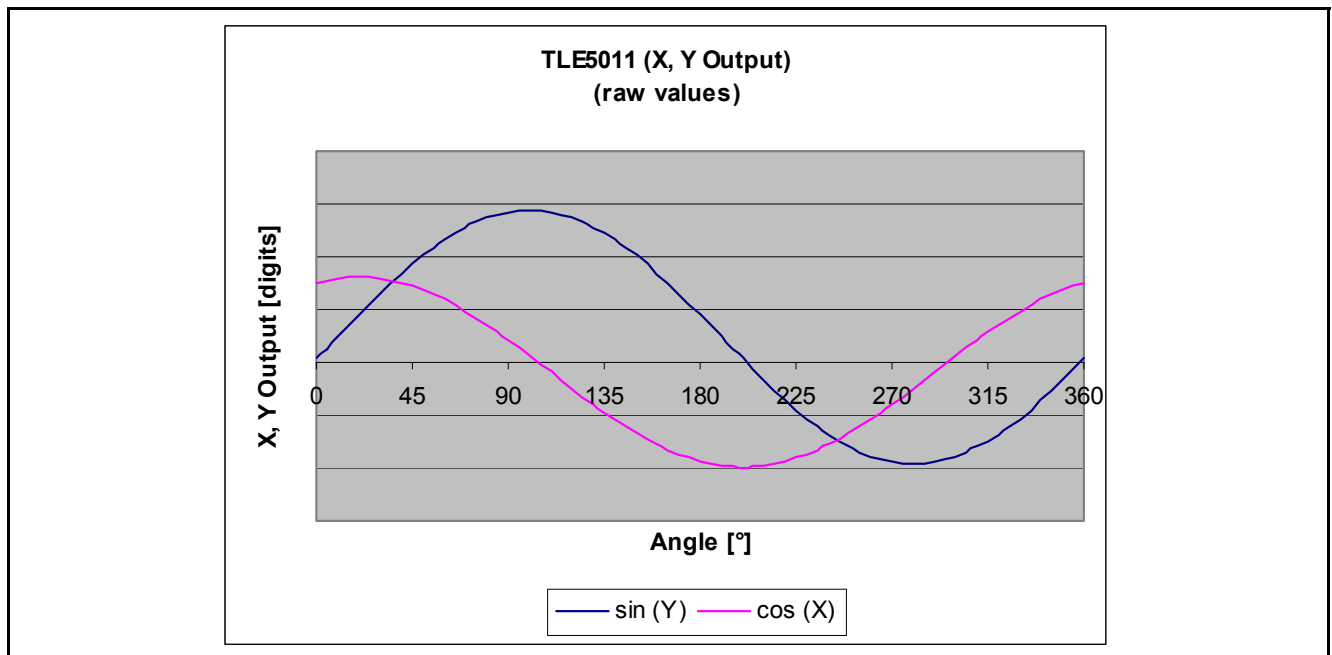
$O_X$  .. Offset of X(COS) signal

$O_Y$  .. Offset of Y(SIN) signal

$\varphi_X$  .. Phase of X(COS) signal

$\varphi_Y$  .. Phase of Y(SIN) signal

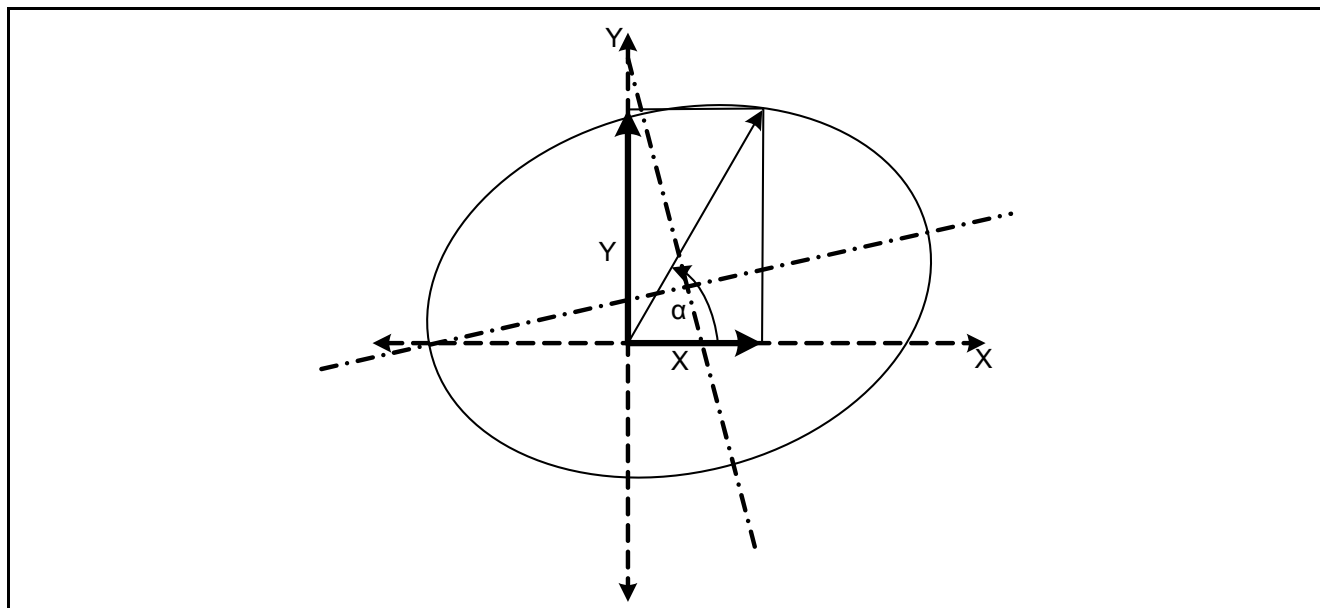
The three parameters that affect the angle calculation are the amplitude, the offset, and the phase. [Figure 1](#) displays the output of X and Y signals. The scale in the figure has been exaggerated to make them easier to see.



**Figure 1** X, Y output signal (raw values)

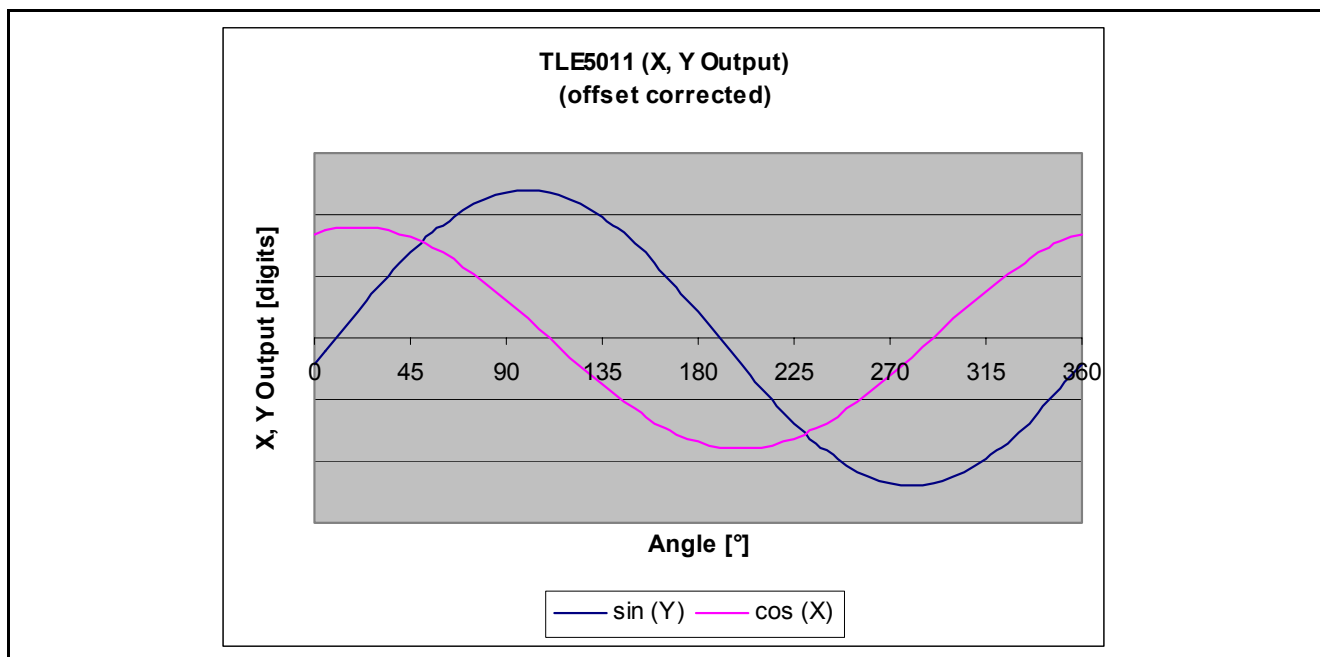
The direct angle calculation ([Equation \(2\)](#)) will result in an elliptical shape ([Figure 2](#)).

$$\alpha = \arctan\left(\frac{Y}{X}\right) \quad (2)$$



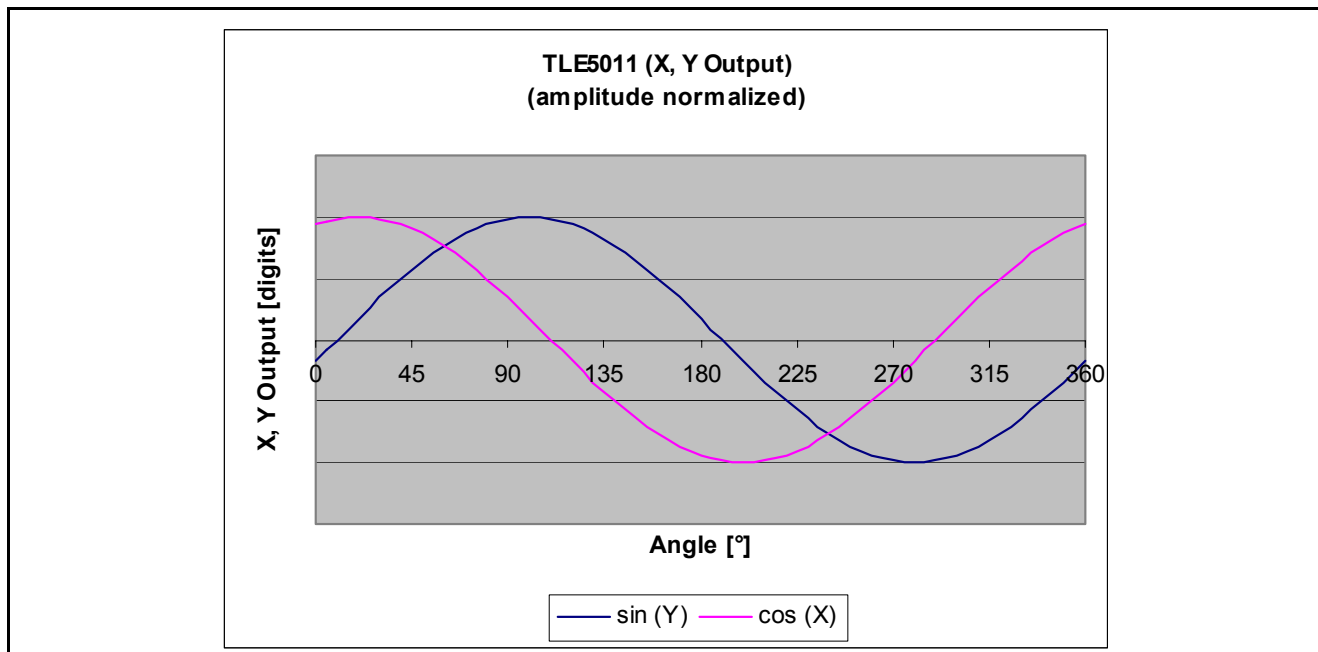
**Figure 2** Angle performance without parameter correction

To minimize the angle error, it is important to achieve a circular shape. Therefore some corrections are necessary. First the offset has to be corrected ([Figure 3](#)).



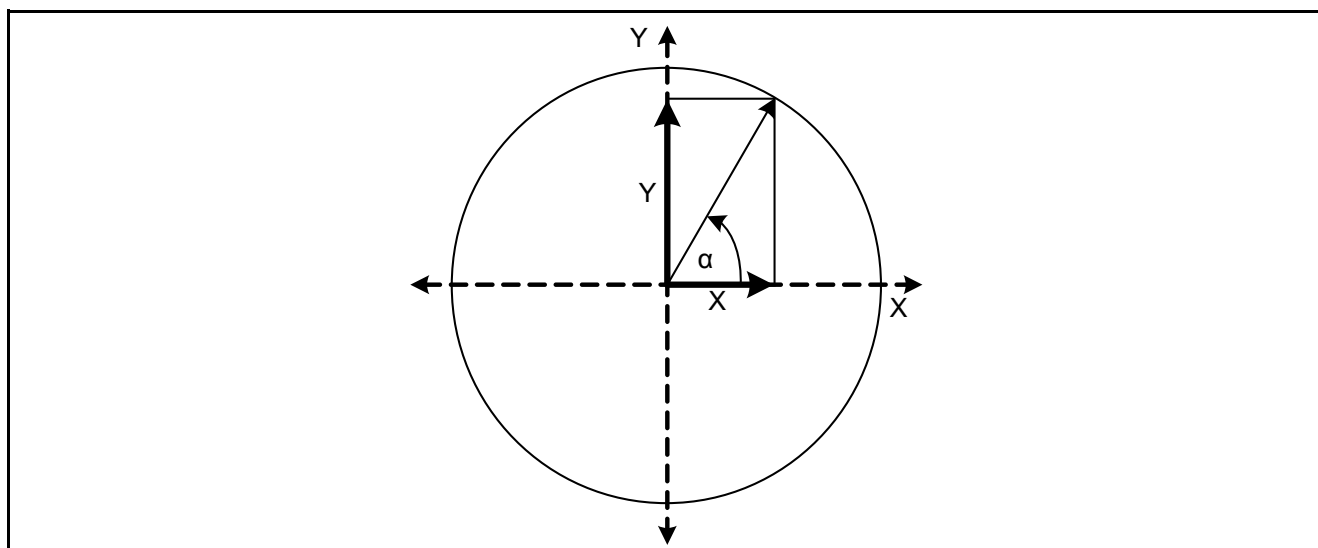
**Figure 3** X, Y output signals (offset corrected)

The next step is the amplitude normalization ([Figure 4](#)), followed by the correction of the non-orthogonality ([Figure 8](#)).



**Figure 4** X, Y output signals (amplitude normalized)

After all corrections have been made, the resulting vector of X and Y signal will have a circular shape.



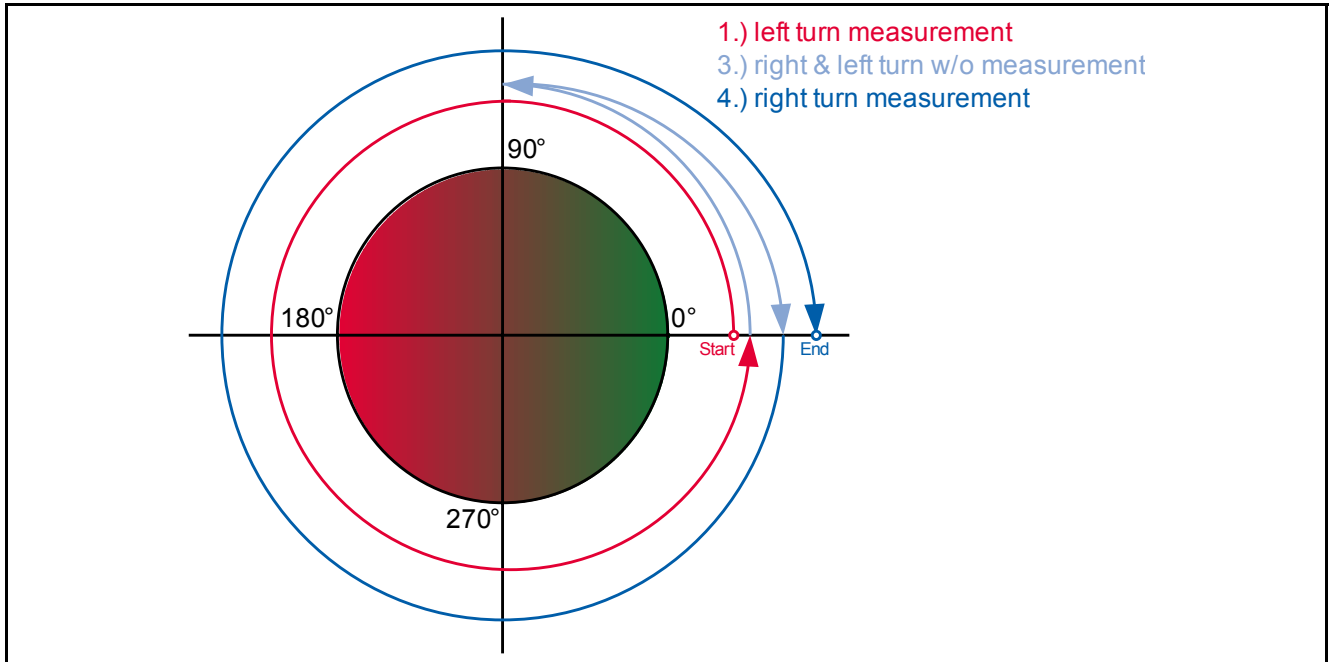
**Figure 5** Angle performance after parameter correction



## 2 Calibration of TLE5011

This chapter explains how to determine the Giant MagnetoResistance (GMR) parameters such as amplitude, offset, and the phase of X- and Y-channels.

The end-of-line calibration can be accomplished using the following sequence (**Figure 6**):



**Figure 6 Calibration routine**

1. Turn magnetic field 360° **left** and measure X and Y values
2. Calculate amplitude, offset, phase correction values of left turn
3. Turn further 90° left and 90° back right without measurement
4. Turn magnetic field 360° **right** and measure X and Y values
5. Calculate amplitude, offset, phase correction values of right turn
6. Calculate **mean** values of amplitude, offset, phase correction

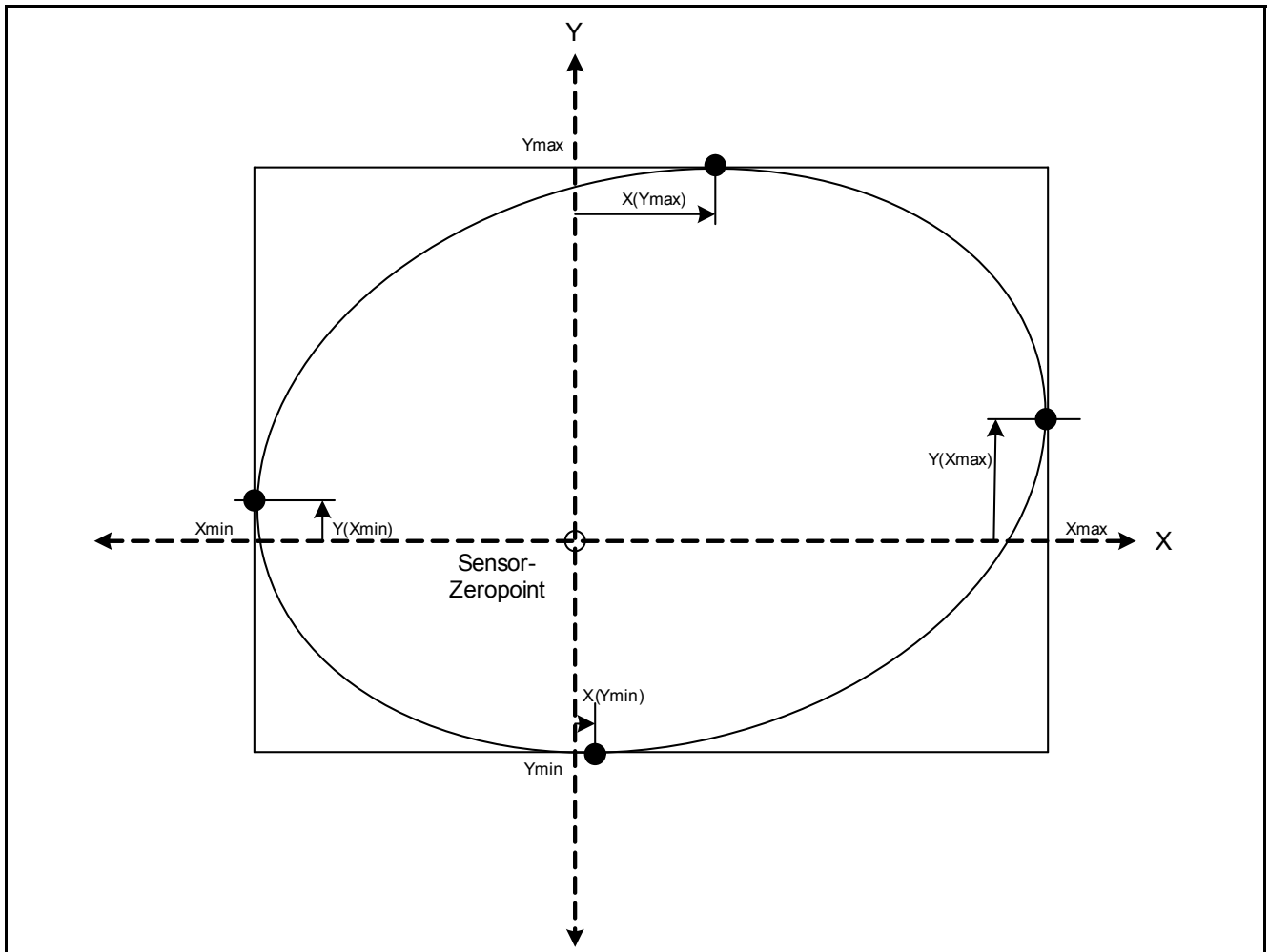
The calibration has to be done at room temperature with a magnet in the specified magnetic field range. The signal amplitude T25 of the temperature measurement path must also be measured afterwards. This is done by setting the TEMP\_EN bit at address 0C<sub>H</sub>. The temperature can then be read out via X-path (XL, XH). Store this value in digits; it is not necessary to convert it into °C.

### 2.1 Extraction of Parameters

There are two possible methods for extracting these parameters. The methods will be discussed in more detail in the next two sections.

#### 2.1.1 Min-Max Method

$X_{\max}$ ,  $X_{\min}$ ,  $Y_{\max}$  and  $Y_{\min}$  have to be extracted out of every full-turn measurement (**Figure 7**).



**Figure 7 Min-Max method**

Afterwards, amplitude ([Equation \(3\)](#), [Equation \(4\)](#)) and offset ([Equation \(5\)](#), [Equation \(6\)](#)) can be calculated:

$$A_X = \frac{X_{\max} - X_{\min}}{2} \quad (3)$$

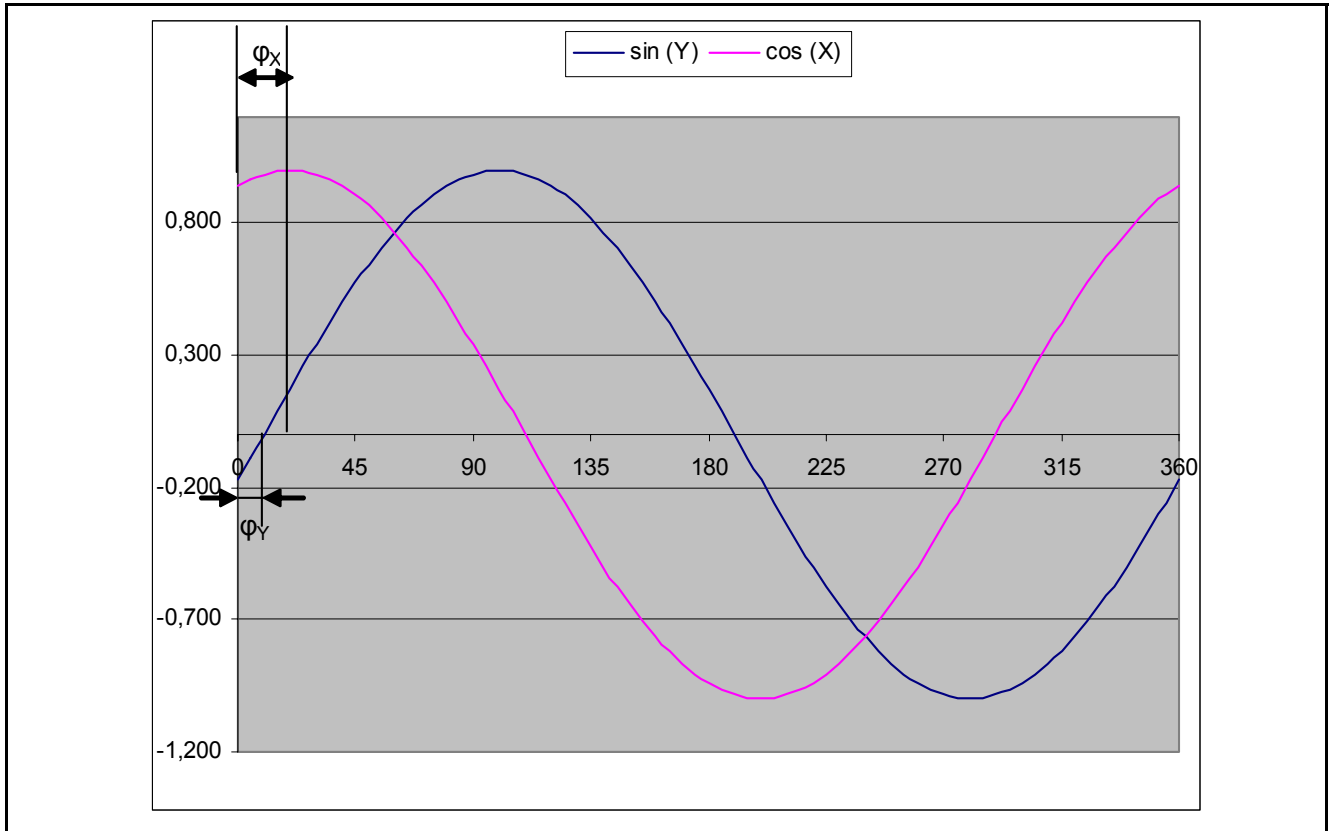
$$A_Y = \frac{Y_{\max} - Y_{\min}}{2} \quad (4)$$

$$O_X = \frac{X_{\max} + X_{\min}}{2} \quad (5)$$

$$O_Y = \frac{Y_{\max} + Y_{\min}}{2} \quad (6)$$

The corresponding maximum and zero-crossing points of the SIN and COS signals do not occur at the precise distance of 90°. The difference between X and Y phases is called the orthogonality error ([Equation \(7\)](#)):

$$\varphi = \varphi_X - \varphi_Y \quad (7)$$



**Figure 8 Orthogonality error**

There is another more accurate way to determine the orthogonality error. The orthogonality can be calculated out of the magnitude of two 90° angle shifted components. Possible angle combinations are 45° and 135°, 135° and 225°, 225° and 315° or 315° and 45°.

The angle value is given by the angle sensor. No reference is necessary. Therefore the final parameters of amplitude and offset ([Chapter 2.2](#)) should be used.

At an angle output of 45° the corresponding Y(sin) and X(cos) values can be read out. This has been done also at 135° ([Figure 9](#)).

Next step is to calculate the length of the magnitudes ([Equation \(8\)](#)):

$$\begin{aligned} M_{45} &= \sqrt{X_{45}^2 + Y_{45}^2} \\ M_{135} &= \sqrt{X_{135}^2 + Y_{135}^2} \end{aligned} \quad (8)$$

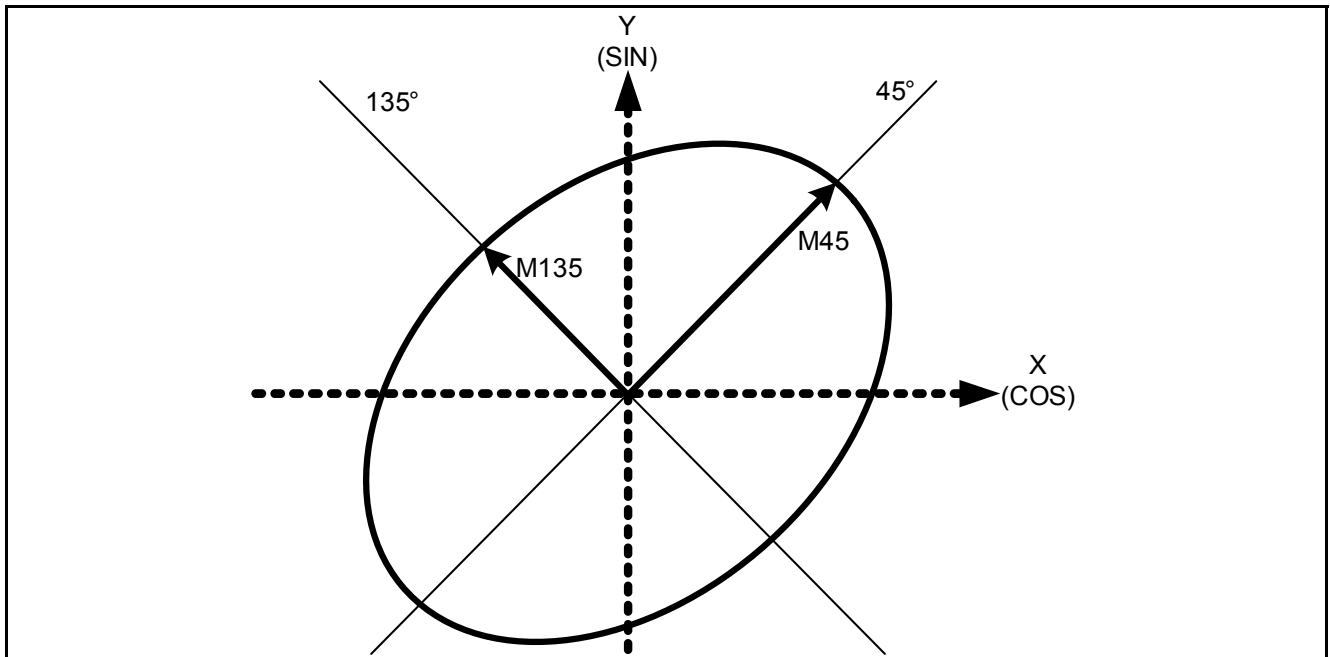
$M_{45}$ ,  $M_{135}$ .. Magnitude at 45° and 135°

$X_{45}$ ,  $X_{135}$  .. Cosine values at 45° and 135°

$Y_{45}$ ,  $Y_{135}$  .. Sine values at 45° and 135°

With these magnitudes the orthogonality can be calculated ([Equation \(9\)](#)):

$$\varphi = 2 * \arctan\left(\frac{M_{135} - M_{45}}{M_{135} + M_{45}}\right) \quad (9)$$



**Figure 9** Correction of orthogonality error

### 2.1.2 Exact Method

This method uses the Discrete Fourier Transform (DFT) to extract the parameters out of the measurements. Therefore an accurate reference system is necessary. This method is done using  $2^m$  measurement points at  $360^\circ$  (e.g.  $m = 8$ ;  $n = 2^m = 2^8 = 64$ ).

#### DFT Offset Calculation:

The offset is calculated by the summation of the X- or Y- measurements divided by the number of measurement points ([Equation \(10\)](#)):

$$\begin{aligned} O_x &= [X(1) + X(2) + \dots + X(n)] / n \\ O_y &= [Y(1) + Y(2) + \dots + Y(n)] / n \end{aligned} \quad (10)$$

$X(n)$  .. X value at measurement point n

$Y(n)$  .. Y value at measurement point n

n .. Measurement points

**DFT Amplitude and Phase Calculation:**

To determine the amplitude, the real and imaginary parts must be calculated. This has been done with **Equation (11)** for the X values and **Equation (12)** for the Y values.  $\beta$  describes the reference angle (e.g.  $n = 64$ ; measurement every  $360^\circ / 64 = 5.625^\circ$  step).

$$\begin{aligned} DFT\_X\_r &= [X(1)*\cos(\beta_1) + X(2)*\cos(\beta_2) + \dots + X(n)*\cos(\beta_n)] * 2/n \\ DFT\_X\_i &= [X(1)*\sin(\beta_1) + X(2)*\sin(\beta_2) + \dots + X(n)*\sin(\beta_n)] * 2/n \end{aligned} \quad (11)$$

$$\begin{aligned} DFT\_Y\_r &= [Y(1)*\cos(\beta_1) + Y(2)*\cos(\beta_2) + \dots + Y(n)*\cos(\beta_n)] * 2/n \\ DFT\_Y\_i &= [Y(1)*\sin(\beta_1) + Y(2)*\sin(\beta_2) + \dots + Y(n)*\sin(\beta_n)] * 2/n \end{aligned} \quad (12)$$

Now the amplitude and phase can be calculated (**Equation (13)**, **Equation (14)**)

$$\begin{aligned} A_X &= \sqrt{(DFT\_X\_r)^2 + (DFT\_X\_i)^2} \\ A_Y &= \sqrt{(DFT\_Y\_r)^2 + (DFT\_Y\_i)^2} \end{aligned} \quad (13)$$

$$\begin{aligned} \varphi_X &= \arctan \frac{DFT\_X\_i}{DFT\_X\_r} \\ \varphi_Y &= \frac{\pi}{2} - \arctan \frac{DFT\_Y\_i}{DFT\_Y\_r} \\ \varphi &= \varphi_X - \varphi_Y \end{aligned} \quad (14)$$

**2.2 Final Parameters**

No matter what calibration method is used, you still have to calculate the symmetrical values of the parameters. This is done using the mean value of the clock-wise (cw) rotation parameters and counterclock-wise (ccw) rotation parameters. This calculation has to be done with X and Y parameters. These parameters have to be used for the signal correction.

$$\begin{aligned} A_M &= \frac{A_{cw} + A_{ccw}}{2} \\ O_M &= \frac{O_{cw} + O_{ccw}}{2} \\ \varphi_M &= \frac{\varphi_{cw} + \varphi_{ccw}}{2} \end{aligned} \quad (15)$$

$(A, O, \varphi)_M$  .. Mean parameters

$(A, O, \varphi)_{cw}$  .. Parameters of clock-wise rotation

$(A, O, \varphi)_{ccw}$  .. Parameters of counterclock-wise rotation

## 2.3 Temperature-dependent Behavior

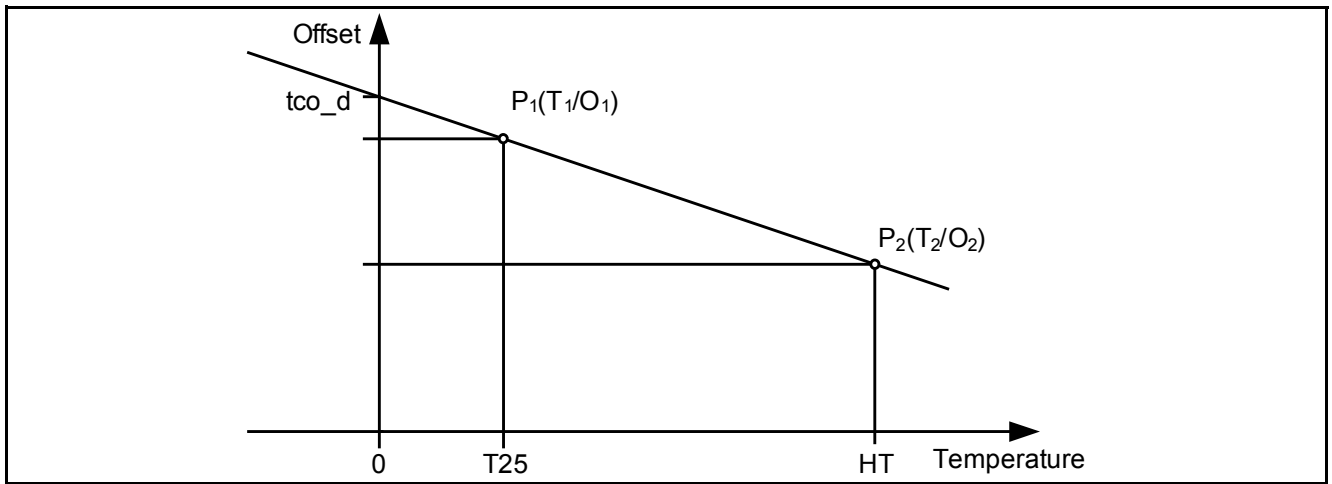
The temperature offset gradients ( $KT_{OX}$ ,  $KT_{OY}$ ) for both channels depend on the value at 25°C. These gradients are necessary for the temperature offset compensation.

$$\begin{aligned} KT_{OX} &= tco\_d\_x + (tco\_k\_x * O_{X25}) \\ KT_{OY} &= tco\_d\_y + (tco\_k\_y * O_{Y25}) \end{aligned} \quad (16)$$

$tco\_d\_x$ ,  $tco\_d\_y$  .. Offset temperature coefficient base (in digits/K)

$tco\_k\_x$ ,  $tco\_k\_y$  .. Offset temperature coefficient gain (in 1/K)

The coefficients ( $tco\_d\_x$ ,  $tco\_d\_y$ ,  $tco\_k\_x$ ,  $tco\_k\_y$ ) have to be determined for every sensor separately. This has been done at two different temperatures (e.g. T25 and HT).



**Figure 10 Temperature coefficients**

The offset of X and Y channels at two temperatures has to be known before the coefficients can be calculated with [Equation \(17\)](#) and [Equation \(18\)](#).

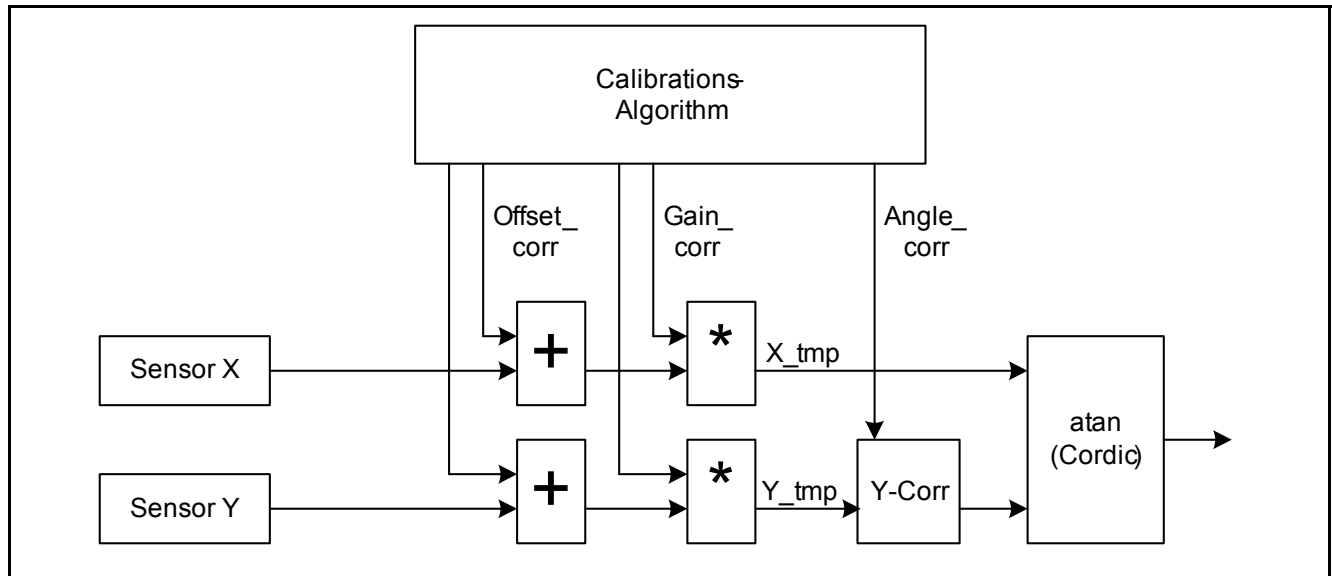
$$tco\_k = \frac{O_2 - O_1}{T_2 - T_1} \quad (17)$$

$$tco\_d = O_1 - tco\_k * T_1 \quad (18)$$

The temperature offset compensation should be used to achieve more accurate angle values over the whole temperature range.

### 3 Angle Calculation

To get highly accurate angle values, the following angle calculation must be performed. **Figure 11** shows the implementation within a microcontroller.



**Figure 11 Implementation of angle calculation**

#### Offset Correction (Offset\_corr)

To increase the accuracy, the temperature-dependent offset drift can be compensated for. The temperature of the chip has to be read out. The offset values  $O_X$  and  $O_Y$  can be described by the following equations:

$$\begin{aligned} O_X &= O_{X25} + \frac{KT_{OX}}{S_T} * (T - T_{25}) \\ O_Y &= O_{Y25} + \frac{KT_{OY}}{S_T} * (T - T_{25}) \end{aligned} \quad (19)$$

$O_{X25}$  .. Offset of X(COS) signal at room temperature (in digits)

$O_{Y25}$  .. Offset of Y(SIN) signal at room temperature (in digits)

$KT_{OX}$  .. Gradient of X-offset (in digits/K)

$KT_{OY}$  .. Gradient of Y-offset (in digits/K)

$S_T$  .. Temperature sensor sensitivity (in digits/K)

$T$  .. Temperature (in digits)

$T_{25}$  .. Temperature at room temperature (in digits)

After the X and Y values are read out, the temperature-corrected offset value must be subtracted (**Equation (20)**):

$$\begin{aligned} X_1 &= X - O_X \\ Y_1 &= Y - O_Y \end{aligned} \quad (20)$$

### Amplitude Normalization (Gain\_corr)

The next step is to normalize the X and Y values by using the mean values determined in the calibration.

$$\begin{aligned} X_2 &= \frac{X_1}{A_{XM}} \\ Y_2 &= \frac{Y_1}{A_{YM}} \end{aligned} \quad (21)$$

### Non-Orthogonality Correction (Angle\_corr)

The influence of the non-orthogonality can be compensated for by using [Equation \(22\)](#), in which only the Y channel must be corrected.

$$Y_3 = \frac{Y_2 - X_2 * \sin(-\varphi)}{\cos(-\varphi)} \quad (22)$$

### Resulting Angle

After correction of all errors, the resulting angle can be calculated using the arctan function<sup>1)</sup>.

$$\alpha = \arctan\left(\frac{Y_3}{X_2}\right) - \varphi_X \quad (23)$$

1) Microcontroller library function "arctan2(Y<sub>3</sub>,X<sub>2</sub>)" works better to resolve 360°



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