Application Note No. 145

Low Cost, 3 V, 2.33 GHz Class A SDARS Active Antenna Amplifier Output Stage using the Infineon BFP450 Transistor

RF & Protection Devices



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1 Low Cost, 3 V, 2.33 GHz Class A SDARS Active Antenna Amplifier Output Stage using the Infineon BFP450 Transistor

Overview

BFP450 SIEGET transistor is investigated as an alternative to the BFP650 SiGe Low Noise Transistor for the output stage of an SDARS active antenna LNA. A key parameter is +20 dBm P_{1dB} capability in the output stage. The PCB used is standard FR4 material & "0402" case sizes components are used. A total of approximately 50 mm² of PCB area is required, the total component count, including the BFP450 and all passives, is 13. Net result is: BFP450 provides slightly more available output power than BFP650 at comparable DC operating points; however, BFP450 has less gain and higher noise figure. See table below. Both devices are in SOT343 package with identical pin-outs. Note output power is "voltage limited" = e.g. if bias resistors were changed after power supply voltage was increased, one should be able to hit +20 dBm OP_{1dB} with less than 100 mA current.

Table 1 Comparison of BFP650 and BFP450 as SDARS active antenna output stage at 2.33 GHz

Device	DC Operating Point	Small Signal Gain, dB	Output P _{1dB} , dBm	Noise Figure, dB
BFP450	3 V, 76 mA, $V_{\rm CE}$ = 2.7 V	9.8	+18.7	2.7
BFP450	3.7 V, 100 mA, $V_{\rm CE}$ = 3.2 V	10.0	+20.5	Not tested
BFP650	3.0 V, 53 mA	14.1	≈ +18.0	1.3

Summary

- Achieved 9.8 dB gain, 2.7 dB Noise Figure over the 2320 2345 MHz band, drawing 76 mA @ 3.0 V, or 100 mA @ 3.7 V. Amplifier is unconditionally stable from 5 MHz to 8 GHz. Output $P_{\rm 1dB}$ = +18.7 dBm @ 3 V, 76 mA or +20.5 dBm @ 3.7 V, 100 mA.
- BFP450 seems to show a slight advantage in Output P_{1dB} as compared to the BFP650. However, gain of BFP450 in same PC board is approx. 4 dB lower, and noise figure of BFP450 is 1.4 dB higher.

Block Diagram of Application

Typical SDARS Active Antenna LNA 2320 - 2332.5 MHz (SIRIUS, 3 Stages) 2332.5 - 2345 MHz (XM Radio, 2 Stages)

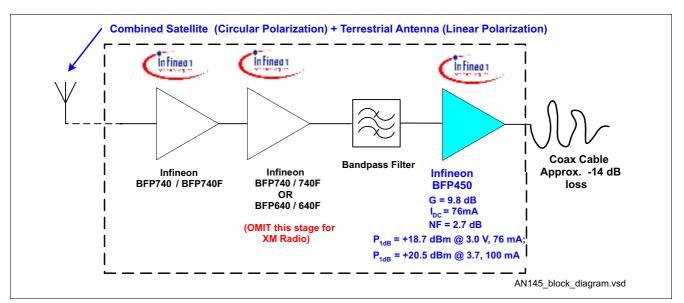


Figure 1 Block Diagram of Application

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PC Board Cross Sectional Diagram

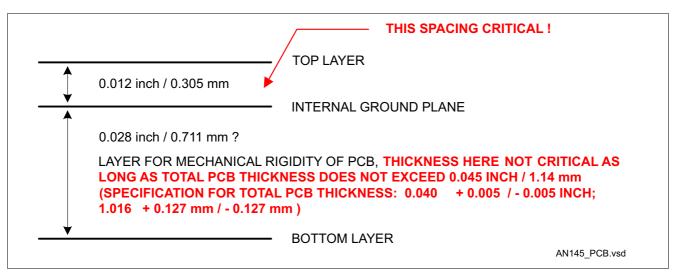


Figure 2 PCB - Cross Sectional Diagram

Schematic Diagram

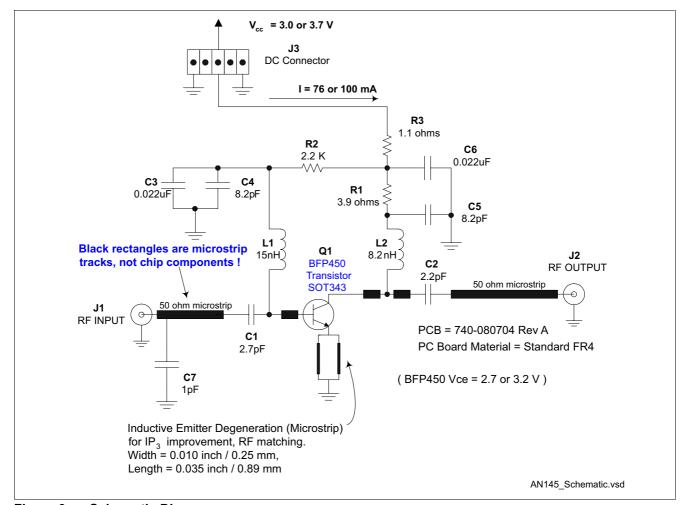


Figure 3 Schematic Diagram

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Summary of Data

T = 25 °C, Network analyzer source power \approx -30 dBm

Table 2 Summary of Results

Parameter	Result	Comments
Frequency Range	Under 2320 to 2345 MHz	Covers both XM Radio and SIRIUS frequency bands.
DC Current	100 mA @ 3.7 V 76 mA @ 3.0 V	Note power supply voltage is measured directly across PCB supply line and ground, to eliminate voltage drop across wire harness.
Gain	9.8 dB @ 2332.5 MHz	
Noise Figure	2.7 dB @ 2332.5 MHz	These values do not extract PCB losses, etc. resulting from FR4 board an passives used on PCB - these results are at input SMA connector.
Input P _{1dB}	+11.7 dBm @ 3.7 V +9.9 dBm @ 3.0 V	Measured @ 2332.5 MHz. See Table 4 and Table 5.
Output P _{1dB}	+20.5 dBm @ 3.7 V +18.7 dBm @ 3.0 V	See Table 4 and Table 5.
Collector Efficiency at 1 dB Compression Point	30.3 % @ 3.7 V 32.5 % @ 3.0 V	Decent results for a Class A amplifier
Input 3 rd Order Intercept	+22.9 dBm @ 2332 MHz	Figure 14 and Figure 15 . Measured at 3.0 V.
Output 3 rd Order Intercept	+32.6 dBm @ 2332 MHz	Figure 14 and Figure 15 . Measured at 3.0 V.
Input Return Loss	9.0 dB @ 2332.5 MHz	
Output Return Loss	9.8 dB @ 2332.5 MHz	
Reverse Isolation	14.6 dB @ 2332.5 MHz	

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Noise Figure, Plot, 2232.5 MHz to 2432.5 MHz, Center of Plot (x-axis) is 2332.5 MHz.

Rohde & Schwarz FSEK3

01 Mar 2005

Noise Figure

EUT Name: BFP450 SDARS Output Stage
Manufacturer: Infineon Technologies
Operating Conditions: V = 3.0 V, I = 76 mA, T = 25 C
Operator Name: Gerard Wevers

Act Conditions: Gerard Wevers

Test Specification: 2.33 GHz SDARS band

Comment: On BFP740 PCB 740-080704 RevA

1 March 2005

<u>Analyzer</u>

 RF Att:
 0.00 dB
 RBW:
 1 MHz
 Range:
 40.00 dB

 Ref LvI:
 -41.00 dBm
 VBW:
 100 Hz
 Ref LvI auto:
 ON

Measurement

2nd stage corr: ON Mode: Direct ENR: HP346A.ENR

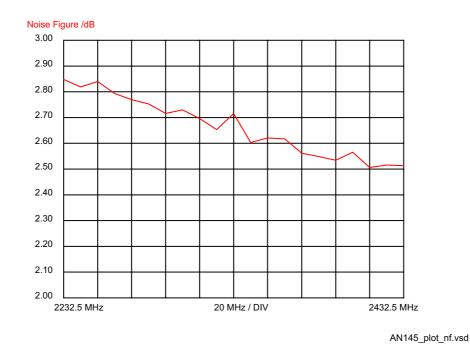


Figure 4 Noise Figure

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Noise Figure, Tabular Data

From Rohde & Schwarz FSEK3 + FSEM30 System Preamplifier = MITEQ SMC-02

Table 3 Noise Figure

Frequency	Noise Figure
2232.5 MHz	2.85 dB
2242.5 MHz	2.82 dB
2252.5 MHz	2.84 dB
2262.5 MHz	2.79 dB
2272.5 MHz	2.77 dB
2282.5 MHz	2.75 dB
2292.5 MHz	2.72 dB
2302.5 MHz	2.73 dB
2312.5 MHz	2.70 dB
2322.5 MHz	2.65 dB
2332.5 MHz	2.72 dB
2342.5 MHz	2.60 dB
2352.5 MHz	2.62 dB
2362.5 MHz	2.62 dB
2372.5 MHz	2.56 dB
2382.5 MHz	2.55 dB
2392.5 MHz	2.53 dB
2402.5 MHz	2.57 dB
2412.5 MHz	2.51 dB
2422.5 MHz	2.52 dB
2432.5 MHz	2.51 dB

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Scanned Image of PC Board



Figure 5 Image of PC Board



Scanned Image of PC Board, Close-In Shot.

Total PCB area used \cong 50 mm².

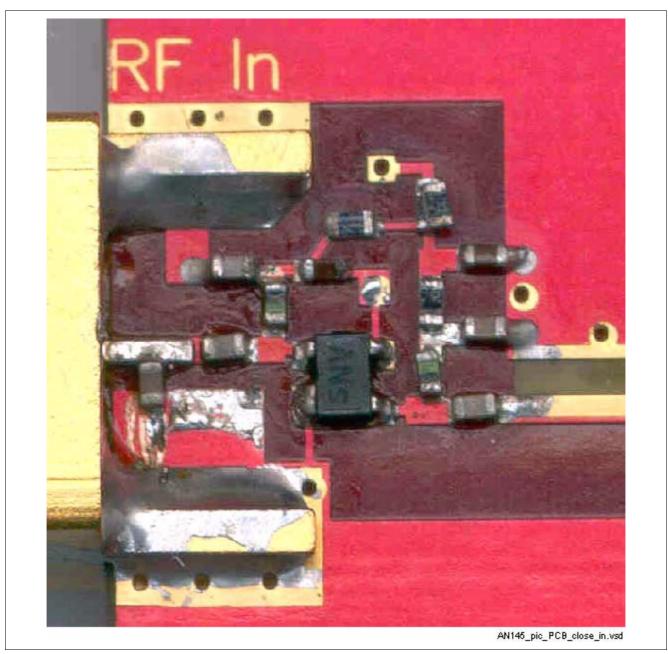


Figure 6 Image of PC Board, Close-In Shot

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Stability

Rohde and Schwarz ZVC Network Analyzer calculates and plots Stabilty Factor "K" in real time. Note minimum K value is approximately 1.04 over the 5 MHz to 8 GHz range. Since inductive emitter degeneration is used, S parameters should be measured up to at least 15 GHz to verify K > 1, $B_1 > 0$ up to 15 GHz.

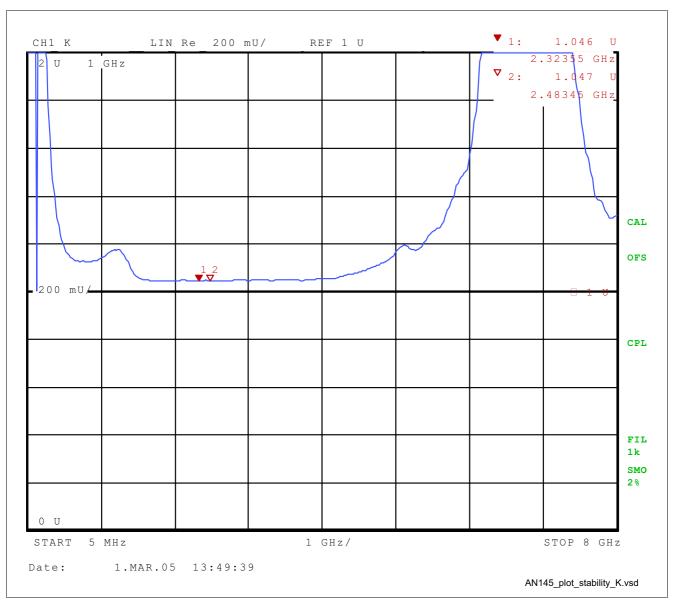


Figure 7 Plot of K(f)

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Gain Compression

Amplifier is checked for 1 dB compression point at $V_{\rm CC}$ = 3.0 V, I = 76 mA (with $V_{\rm CE}$ = 2.7 V), and at $V_{\rm CC}$ = 3.7 V, I = 100 mA (with $V_{\rm CE}$ = 3.2 V). An Agilent power meter was used to ensure accurate power levels are measured (as opposed to using Vector Network Analyzer in "Power Sweep" mode).

For 3.0 V power supply voltage \Rightarrow $O_{\text{P1dB}} \cong$ +18.7 dBm, or 74.1 mW Collector efficiency at this point is 74.1 mW / (3 V x 76 mA) = 32.5 %

For 3.7 V power supply voltage \Rightarrow $O_{\rm P1dB}$ \cong +20.5 dBm, or 112.2 mW Collector efficiency at this point is 112.2 mW / (3.7 V x 100 mA) = 30.3 %

Table 4 3.0 V, 76 mA

P_{IN} , dBm	P_{OUT} , dBm	Gain	
0	+9.9	9.9	
+5.0	+14.8	9.8	
+6.0	+15.8	9.8	
+7.0	+16.6	9.6	
+8.0	+17.5	9.5	
+9.0	+18.2	9.2	
+10.0	+18.8	8.8	
+11.0	+19.2	8.2	

Table 5 3.7 V, 100 mA

P_{IN} , dBm	P_{OUT} , dBm	Gain	
0	+10.1	10.1	
+5.0	+15.0	10.0	
+6.0	+16.0	10.0	
+7.0	+16.9	9.9	
+8.0	+17.8	9.8	
+9.0	+18.7	9.7	
+10.0	+19.5	9.5	
+11.0	+20.3	9.3	
+12.0	+20.9	8.9	

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Please Note - all plots are taken from ZVC Network Analyzer with amplifier DC bias set to 3.0 V, 76 mA.

Input Return Loss, Log Mag

5 MHz - 8 GHz

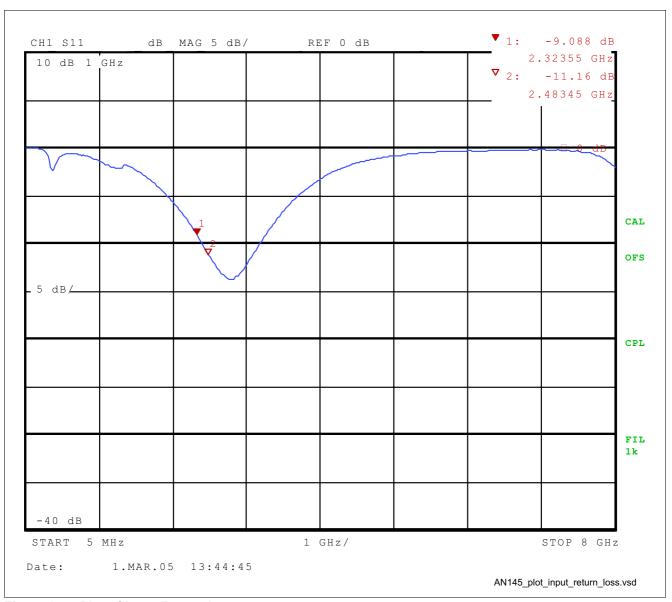


Figure 8 Plot of Input Return Loss

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Input Return Loss, Smith Chart

Reference Plane = Input SMA Connector on PC Board 5 MHz - 8 GHz

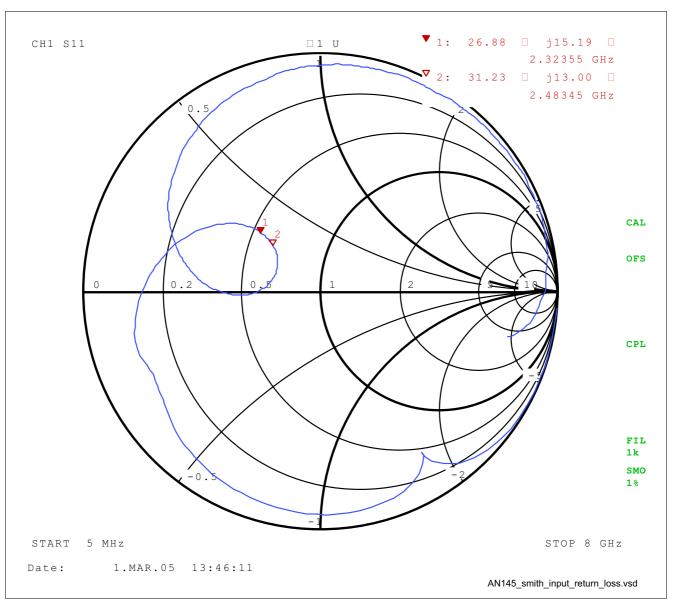


Figure 9 Smith Chart of Input Return Loss

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Forward Gain, Wide Sweep

5 MHz - 8 GHz

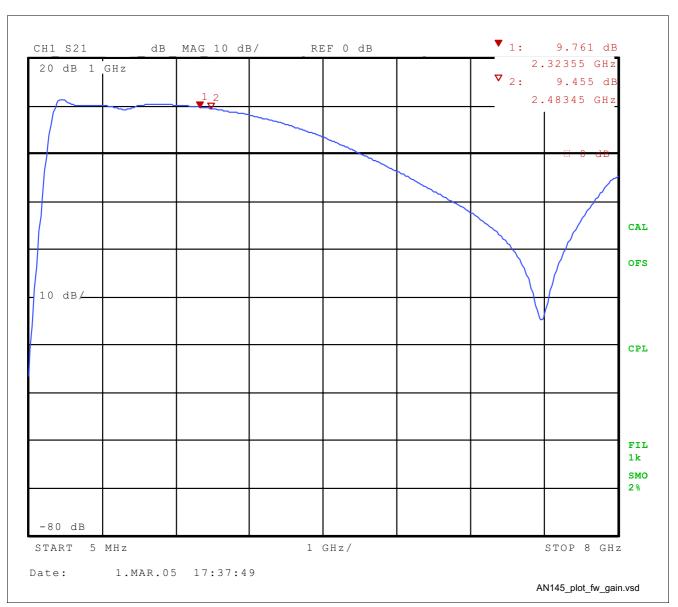


Figure 10 Plot of Forward Gain

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Reverse Isolation

5 MHz - 8 GHz

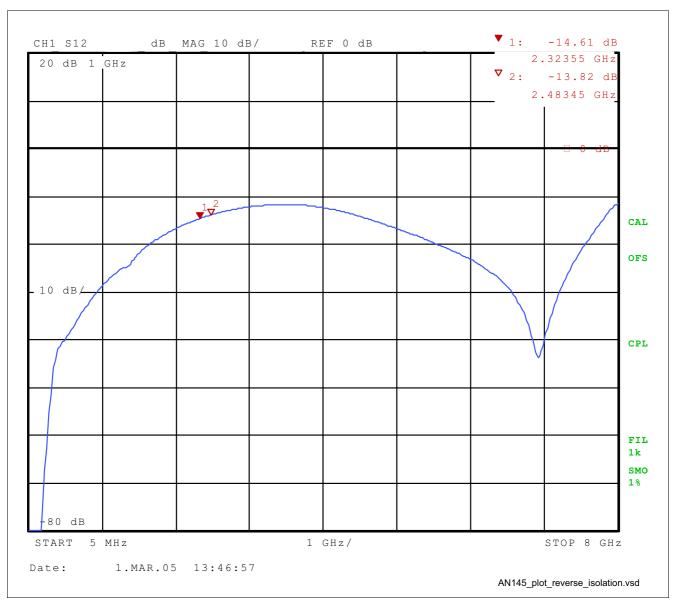


Figure 11 Plot of Reverse Isolation

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Output Return Loss, Log Mag

5 MHz - 8 GHz

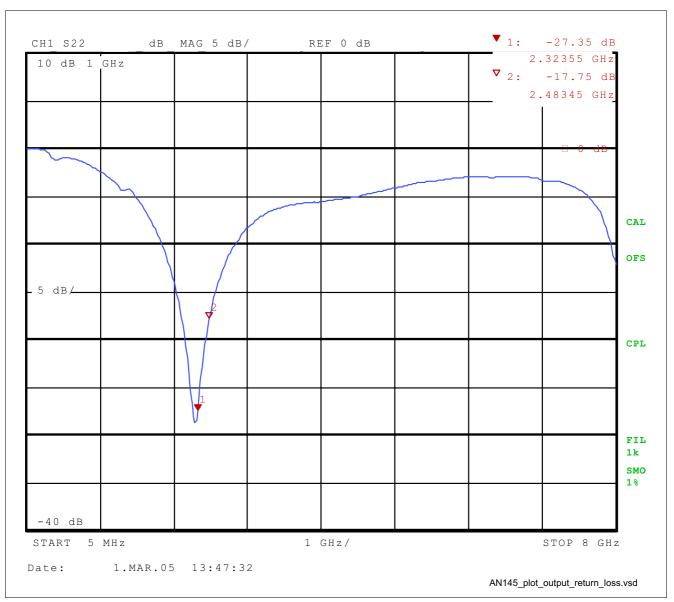


Figure 12 Plot of Output Return Loss

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Output Return Loss, Smith Chart

Reference Plane = Output SMA Connector on PC Board 5 MHz - 8 GHz

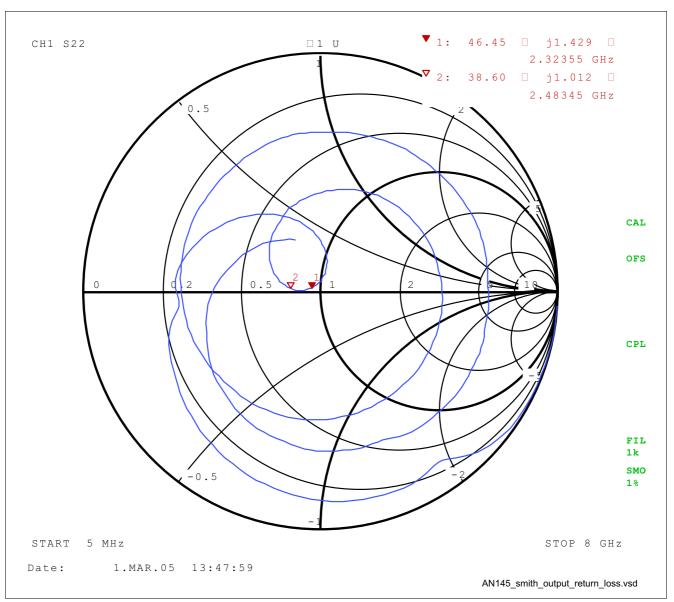


Figure 13 Smith Chart of Output Return Loss

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Two Tone Test

Input Stimulus for Amplifier Two-Tone Test: f_1 = 2332 MHz, f_2 = 2333 MHz, -10 dBm each tone.

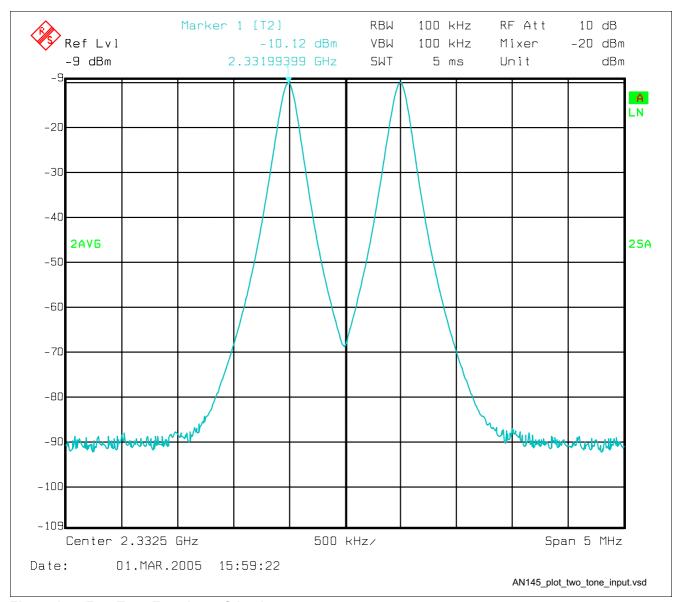


Figure 14 Tow-Tone Test, Input Stimulus

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LNA Response to Two Tone Test

3.0 V, 76 mA for LNA. Input IP_3 = -10 + (65.5 / 2) = +22.8 dBm Output IP_3 = +22.8 dBm + 9.8 dB gain = +32.6 dBm

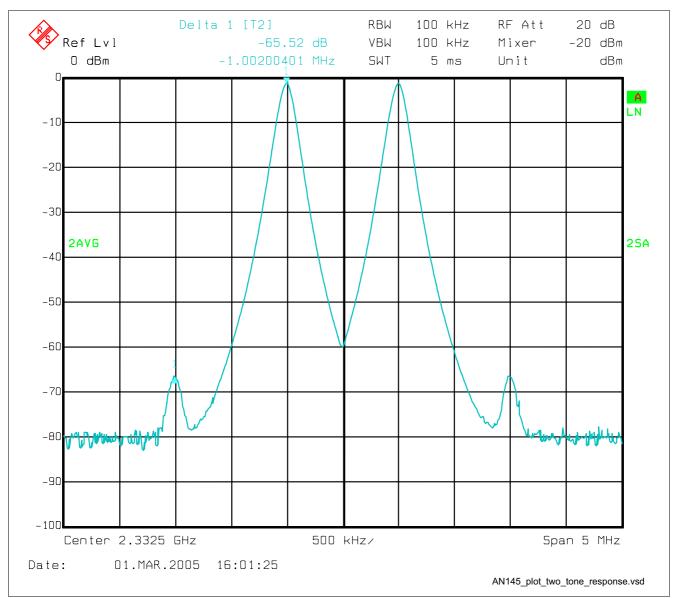


Figure 15 Tow-Tone Test, LNA Response

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