

# Application Note No. 013

800 - 1000 MHz PIN-Diode Transmit-Receive  
Switch

RF & Protection Devices



Never stop thinking

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**800 - 1000 MHz PIN-Diode Transmit-Receive Switch**

**Revision History: 2006-10-20, Rev. 2.0**

**Previous Version: 2000-07-27**

<b>Page</b>	<b>Subjects (major changes since last revision)</b>
All	Document layout change

# 1 800 - 1000 MHz PIN-Diode Transmit-Receive Switch

This application is designed to serve as a non mechanical transmit-receive switch for AMPS, GMS and PDC mobile telephones.

### Advantages

- No power consumption in receive state
- No negative voltage required
- Low component count
- Low cost

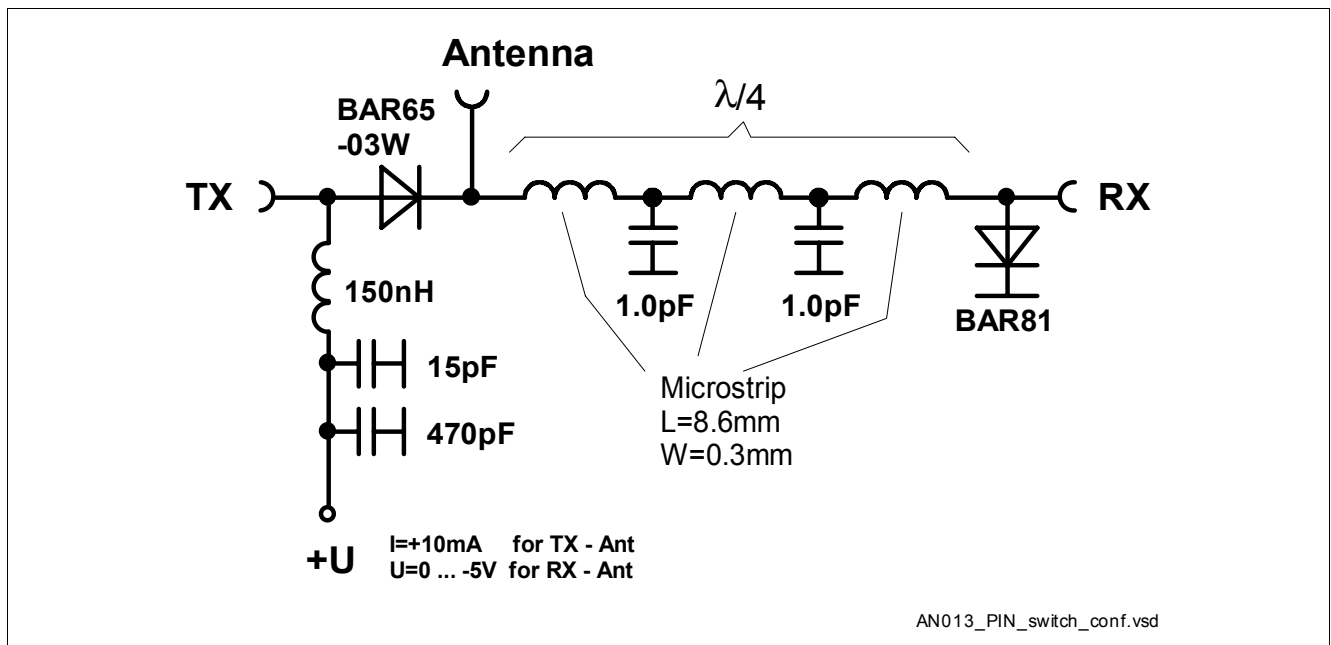


Figure 1 PIN diode switch configuration

Table 1 Performance Data at 800 - 1000 MHz

Transmit-state (I = +10 mA ... 1 mA)		Receive-state (U = -5 V)	
TX-Ant. Loss	0.3 ... 0.4 dB <sup>1)</sup>	RX-Ant. Loss	0.55 ... 0.6 dB <sup>1)</sup>
Ant.-RX Isolation	35 ... 32 dB	TX-RX Isolation	17 ... 16 dB
TX-RX Isolation	35 ... 33 dB	TX-Ant. Isolation	19 ... 17 dB

1) These values are the overall losses, evaluation of a dummy-circuit with diodes replaced by open / short show 0.15 dB loss in TX-Antenna path and 0.2 dB from Antenna to RX.

## 2 Harmonic Distortion Characteristics Measurements

### 2.1 Measurement Setup

TX-Port:  $f = 890 \text{ MHz}$ , 33 dBm power, harmonic suppression  $> 95 \text{ dBc}$

RX-Port: DC- blocked  $50 \Omega$  termination

Ant.-Port: DC-blocked spectrum analyzer

Values referred to input power level at TX-Port:

**Table 2** Input power level at TX-Port

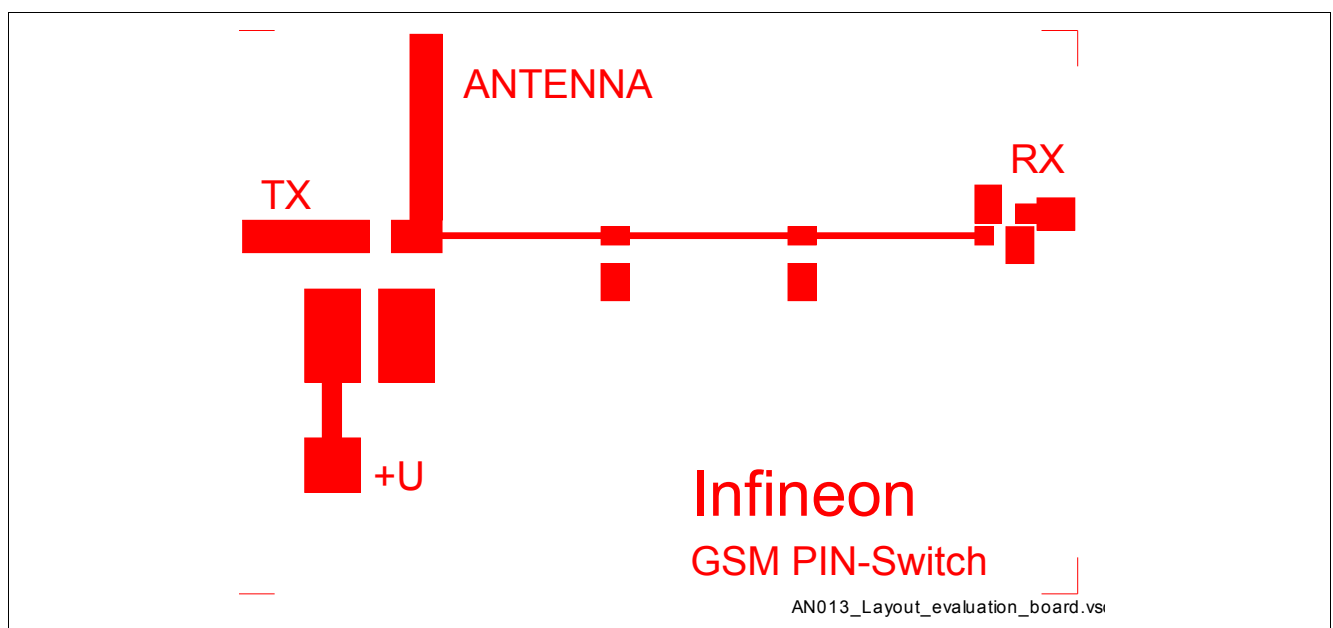
	1. Harmonic @ 1.78 GHz	2. Harmonic @ 2.67 GHz
$I = 5 \text{ mA}$	72 dBc	$> 95 \text{ dBc}$
$I = 10 \text{ mA}$	75 dBc	$> 95 \text{ dBc}$

### 2.2 Functional Description

- In transmit mode both diodes are forward biased and therefore conduct. The short-circuit BAR80 diode at the RF-port is transformed into an open-circuit at the Antenna-port by a  $\lambda/4$  line.
- In receive mode, both diodes are reverse biased and therefore non conducting. The RF signal passes from Antenna- to RX-port via  $\lambda/4$  line.

Further improvement of the circuit can be achieved by compensation of the remaining diode-capacitance in off-state with shunt-inductors.

The  $\lambda/4$  line is realized by microstripline inductors and SMD capacitors to reduce the length of the assembly.



**Figure 2** Layout of the evaluation board (size: 30 mm x 45 mm)

Harmonic Distortion Characteristics Measurements

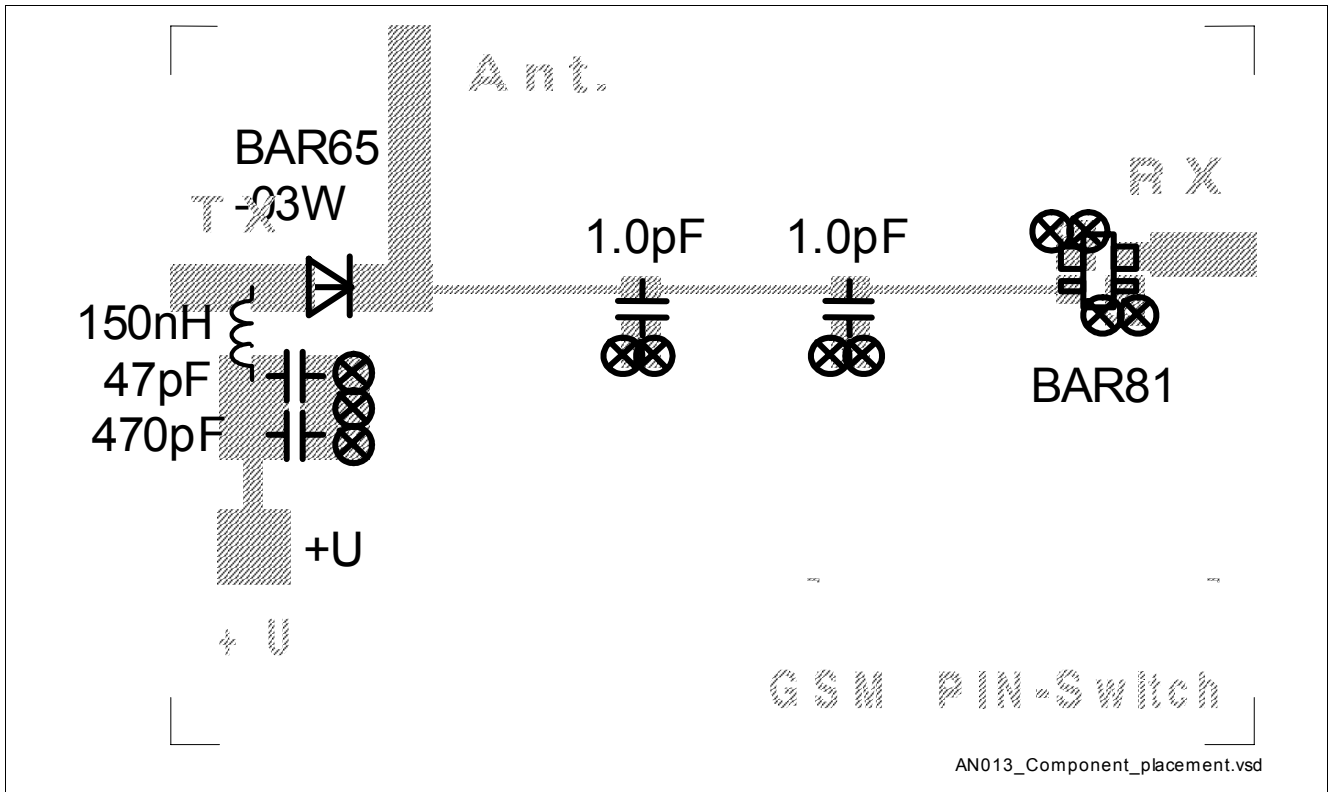


Figure 3 Component placement

Table 3 Part List

BAR81	PIN diode	MW-4	Infineon
BAR65-03W	PIN diode	SOD323	Infineon
1.0 pF	Cap.	0805	S+M
15 pF	Cap.	0805	S+M
470 pF	Cap.	0805	S+M
150 nH	Ind.	SIMID01	S+M
Board	1 mm Epoxy FR4, 30 x 45 mm		



Harmonic Distortion Characteristics Measurements

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kap: 1.0PF ; Capacitor to simulate quater lambda line
ll: 8.6MM ; length of trl (inductor) to simulate quater lambda li
br: 0.3mm ; width of trl (inductor) to simulate quater lambda lir
w50: 1.75mm ; width of 50 ohm line

BLK ; RX-ANT ON, TX-ANT OFF
trl 1 5 w=w50 p=4.85mm sub
trl 5 7 w=w50 p=2.0mm sub
ost 7 w=w50 p=0.6mm sub
one 7 8 b65of ; BAR65-03W
ost 8 w=w50 p=0.6mm sub
trl 8 9 w=w50 p=1.0mm sub
tee 9 10 11 w1=w50 w2=w50 w3=w50 sub
trl 11 2 w=w50 p=10mm sub

step 10 15 w1=w50 w2=br sub
trl 15 20 w=br p=11 sub
tee 20 30 40 w1=br w2=br w3=1.0mm sub
cap 40 50 c=kap
via 50 d=0.5mm sub
via 50 d=0.5mm sub
trl 30 60 w=br p=11 sub
tee 60 70 80 w1=br w2=br w3=1.0mm sub
cap 80 90 c=kap
via 50 d=0.5mm sub
via 50 d=0.5mm sub
trl 70 100 w=br p=11 sub
step 100 110 w1=br w2=1mm sub
trl 110 115 w=1mm p=1mm sub
ost 115 w=1mm p=0.6mm sub
two 115 120 130 b81of ; BAR81
ost 120 w=1mm p=0.6mm sub
via 130 d=0.5mm sub
via 130 d=0.5mm sub
trl 120 140 w=1mm p=1.2mm sub
step 140 150 w1=1mm w2=w50 sub
trl 150 3 w=w50 p=3mm sub
rxan: 3por 1 2 3 ; 1=TX 2=ANT 3=
END

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Figure 6 Simulation Data 1



Harmonic Distortion Characteristics Measurements

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BLK      ; RX-ANT OFF, TX-ANT ON
  trl    1 5      w=w50    p=4.85mm    sub
  trl    5 7      w=w50    p=2.0mm    sub
  ost    7      w=w50    p=0.6mm    sub
  one    7 8      b65on                                ; BAR65-03W
  ost    8      w=w50    p=0.6mm    sub
  trl    8 9      w=w50    p=1.0mm    sub
  tee    9 10 11  w1=w50   w2=w50   w3=w50    sub
  trl    11 2     w=w50    p=10mm    sub
  step   10 15    w1=w50   w2=br     sub
  trl    15 20    w=br     p=11      sub
  tee    20 30 40 w1=br    w2=br     w3=1.0mm sub
  cap    40 50    c=kap                                sub
  via    50      d=0.5mm                                sub
  via    50      d=0.5mm                                sub
  trl    30 60    w=br     p=11      sub
  tee    60 70 80 w1=br    w2=br     w3=1.0mm sub
  cap    80 90    c=kap                                sub
  via    50      d=0.5mm                                sub
  via    50      d=0.5mm                                sub

  trl    70 100   w=br     p=11      sub
  step   100 110  w1=br    w2=1mm    sub
  trl    110 115  w=1mm    p=1mm    sub
  ost    115     w=1mm    p=0.6mm  sub
  two    115 120 130 b81on                                ; BAR81
  ost    120     w=1mm    p=0.6mm  sub
  via    130     d=0.5mm                                sub
  via    130     d=0.5mm                                sub
  trl    120 140  w=1mm    p=1.2mm  sub
  step   140 150  w1=1mm   w2=w50   sub
  trl    150 3    w=w50    p=3mm    sub
txan:   3por 1 2 3 ; 1=TX 2=ANT 3

END

FREQ
STEP    10MHz  2GHZ  10MHz
END

DATA
SUB:  MS  H=1mm  ER=4.8  TAND=0.02  MET1=CU 35UM
b81of:DUMMY      FILE=a:\bar81\mv5v00u0.s2p
b81on:DUMMY      FILE=a:\bar81\mvv0010m.s2p
b65of:DUMMY      FILE=a:\bar65-3w\5w5v00u0.s1p
b65on:DUMMY      FILE=a:\bar65-3w\5wv0010m.s1p
END

```

AN013\_Discription\_file\_simulation2.vsd

Figure 7 Simulation Data 2

Harmonic Distortion Characteristics Measurements

The simulation shows the following results:

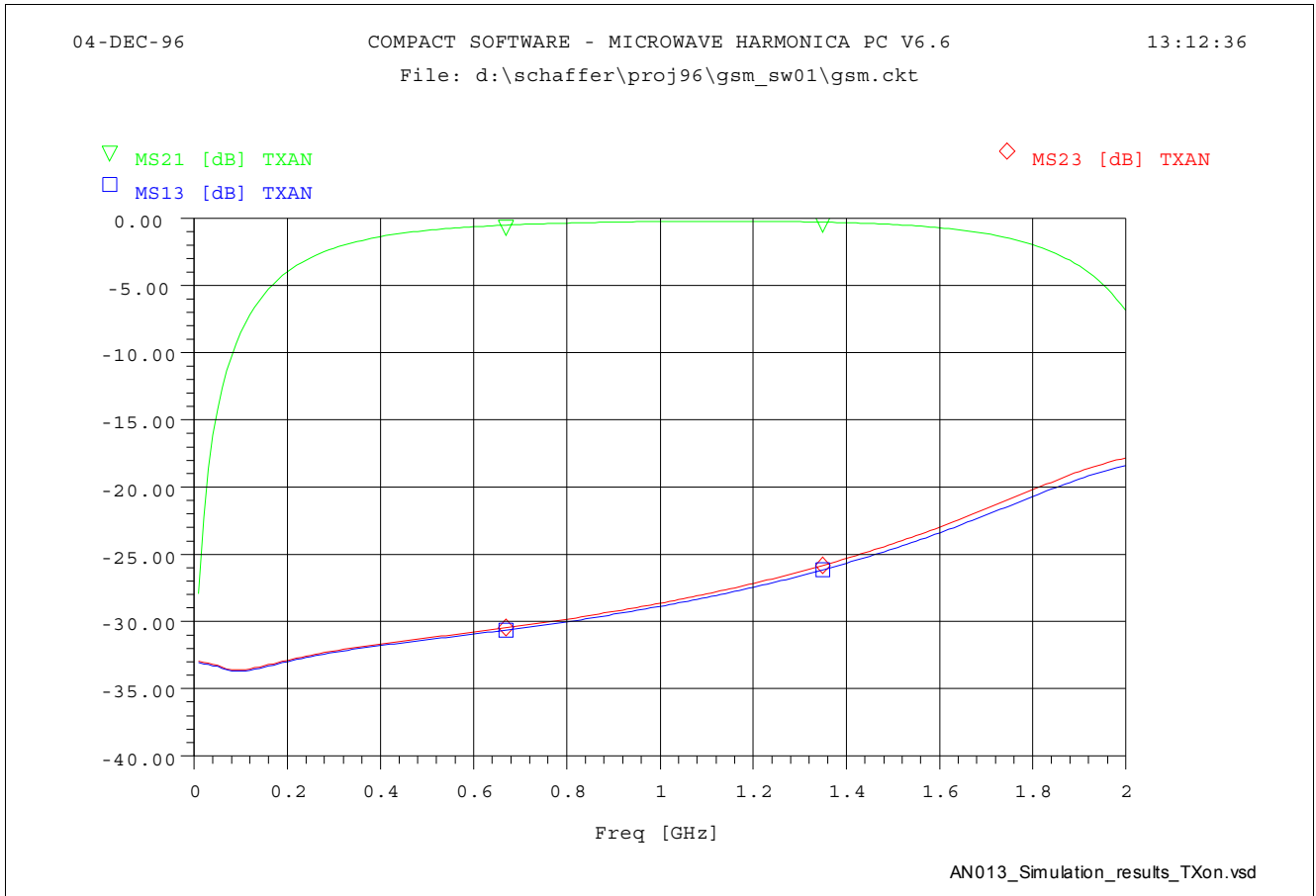


Figure 8 Simulation results: State 'TX on'

Harmonic Distortion Characteristics Measurements

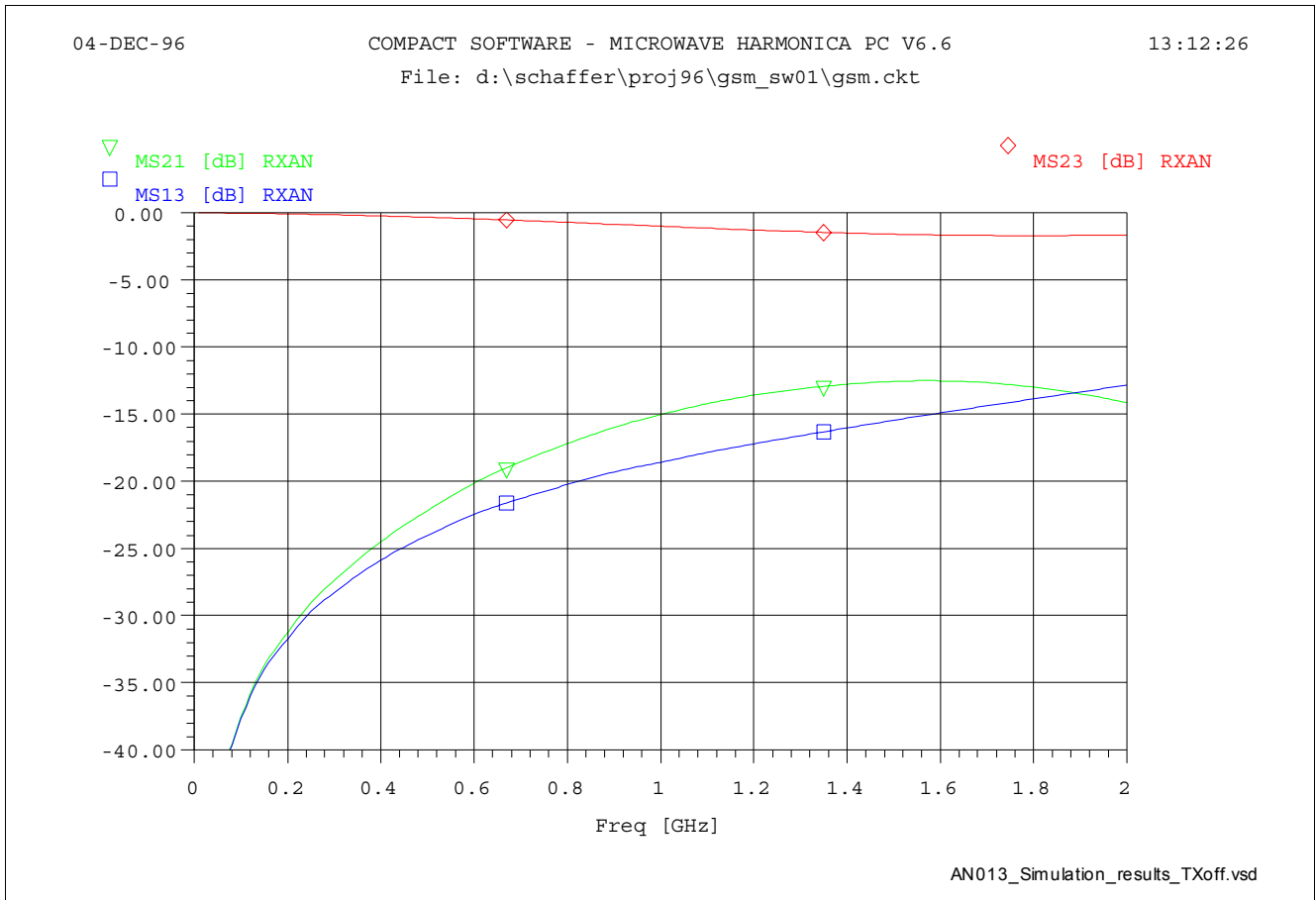


Figure 9 Simulation results: 'TX off'