

Simple and cost effective dimming solutions

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With an existing 8-pin, non-dimming lighting ballast controller (for example, the IR2520D from International Rectifier, shown in Figures 1 and 2) only two pins are used (FMIN and VCO) to deal with preheat, ignition and running requirements of the fluorescent lamp. The remaining pins perform standard functions such as IC supply and ground (pins VCC and COM), plus high- and low-side gate drive for the half-bridge (pins LO, VS, HO and VB).

The schematic diagram illustrates the internal architecture of the 120-µA, 100-MHz, 10-bit SAR ADC. Key components include:

- Power Supplies:** VCC (15.6V), COM, VCO (5.1V), and FMIN (5V).
- Bootstrap FET and Bootstrap FET Control:** A block for managing the bootstrap FET, which is used to charge the sampling capacitor.
- High-Voltage Well:** A well containing the 10-bit SAR ADC core, which includes a 300ns PGEN input, a 1us blank input, and a 120µA current source.
- Level-Shift FETs:** Used to shift the input signal to the ADC core.
- Driver Logic:** A block that drives the input of the ADC core.
- Level Shift PGEN:** A block that generates the PGEN signal for the level shift FETs.
- Level-Shift FETs:** Two FETs used to shift the input signal to the ADC core.
- VS-Sensing FET:** A FET used for sensing the input voltage.
- Averaging Circuit x5:** A circuit that averages the input signal over 5 samples.
- 120µA Current Source:** A current source used for the averaging circuit.

All values are typical.

for the IC, maintaining the VCC at the internal clamp voltage. A small internal current source at the VCO pin slowly charges up an external capacitor causing the voltage on the VCO pin to ramp up linearly. This in turn ramp downs the frequency of the gate driver outputs (LO and HO), and the half-bridge switching circuit from

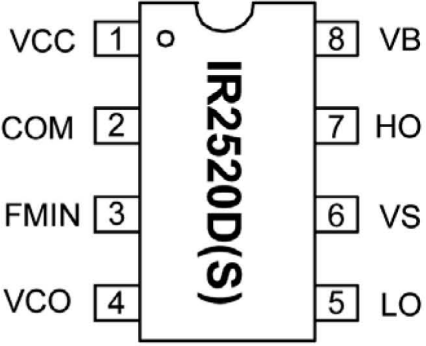
Symbol	Description		
VCC	Supply voltage		
COM	IC power and signal ground		
FMIN	Minimum frequency setting		
VCO	Voltage controlled oscillator input		
LO	Low-side gate driver output		
VS	High-side floating return		
HO	High-side gate driver output		
VB	High-side gate driver floating supply		

Figure 2: Lead assignment for IR2520D

its maximum starting value. The lamp voltage increases as the frequency ramps down towards the resonance frequency of the high-Q, under-damped output stage. The VCO pin voltage continues to increase and the frequency keeps decreasing until the lamp ignites. The output circuit then becomes an over-damped, low-Q circuit. The VCO voltage increases, causing the IC to enter run mode. The frequency level stops decreasing once the VCO pin surpasses 5V and stays at the minimum frequency as programmed by an external resistor on the FMIN pin.

With demand for dimming functionality becoming ever greater, but engineers not wanting to sacrifice the advantages of compact low pin count devices like the IR2520D, a way to control dimming through the pins already available needed to be found. As the VCO pin is required to perform the necessary frequency sweep for preheat and ignition, the FMIN pin was left as the only viable option through which this could be accomplished.

Dimming control through a single pin

The dimming of a fluorescent lamp

can be achieved by using operating frequency to control the current being applied to the lamp. As the frequency of the half-bridge is increased, the gain of the resonant tank circuit decreases and the lamp current lowers. It is possible to regulate the lamp current to a dimming reference level by continuously adjusting the half-bridge frequency through closed-loop feedback circuit. Dimming is enabled by combining the AC lamp current measurement with a DC reference voltage at a single node. The AC lamp current is measured across sensing resistor RCS and coupled onto the DC dimming reference via feedback capacitor CFB and resistor RFB.

The feedback circuit regulates the valley of the AC+DC signal to COM as the DC dimming level is raised or lowered by continuously adjusting the half-bridge frequency. This causes the amplitude of the lamp current to then increase or decrease so that dimming can be carried out. If the DC reference is increased, the valley of the AC+DC signal will rise above COM and the feedback circuit will lower the frequency in order to enlarge the gain of the resonant tank. This will raise the lamp current, as well as the amplitude

of the AC+DC signal at the DIM pin, until the valley reaches COM again. If the DC reference is decreased, the valley will decrease below COM. The feedback circuit will then increase the frequency to lower the resonant tank gain until the valley reaches COM again. The IR2520D's FMIN pin, used to program a single running frequency, has now been replaced with a DIM pin, which measures the AC+DC signal for dimming.

The IRS2530D dimming control IC offers a complete 8-pin solution that contains all dimming ballast functions. The VCO pin includes the frequency sweep timing control for preheat and ignition, and also programs the loop speed for the dimming feedback circuit during dim mode.

When a voltage is first applied to VCC (14V, typical) the IC exits UVLO mode and enters preheat/ignition mode. The half-bridge begins oscillating at the maximum frequency and the internal current source at the VCO pin begins charging up an external capacitor (CVCO) linearly from COM. The output frequency decreases as the VCO voltage increases and the lamp filaments are preheated by sec-

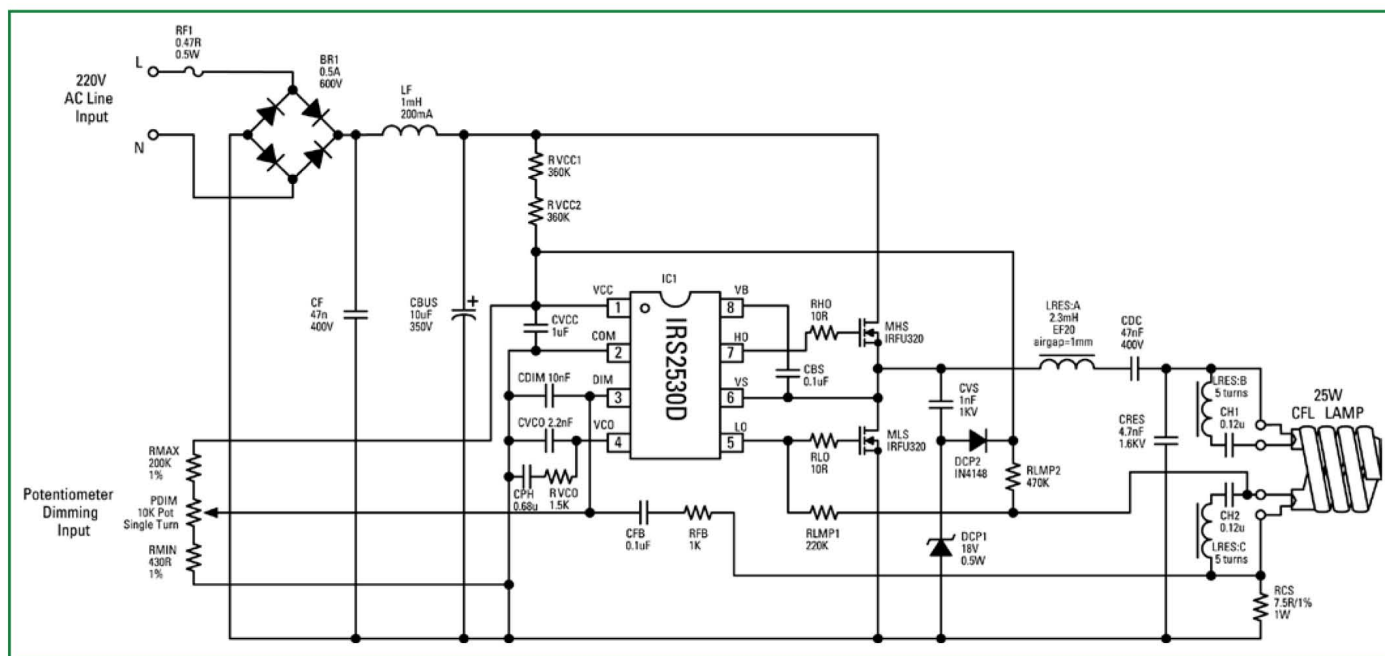


Figure 3: Dimming mini-ballast circuit using the IRS2530D

ondary windings from the resonant tank inductor. As the VCO voltage charges up, the frequency decreases towards the resonance frequency of the resonant tank circuit and the output voltage across the lamp increases. The lamp ignites when the output voltage exceeds the lamp ignition threshold voltage, lamp current begins to flow, and the IC enters dim mode.

A schematic showing a complete dimming mini-ballast circuit is described in Figure 3. It is designed to run from a 220VAC line and to drive a 25W compact fluorescent lamp. The 220VAC/50Hz line input voltage is full-wave rectified (BR1) and then goes through the EMI filter (CF and LF) before being smoothed by the DC bus capacitor (CBUS). The half-bridge switches (MHS and MLS), which are controlled by the IRS2530D, allow preheating, igniting and dimming of the lamp. RVCC1 and RVCC2 provide the micro-power start-up current for the IC's VCC supply, and the charge pump (CS-

NUB, DCP1 and DCP2) takes over as the IC supply once the half-bridge begins to oscillate. The resonant tank circuit (LRES and CRES) provides the transfer function for generating the high voltages needed for lamp ignition and low-pass filtering for dimming. Secondary windings from the resonant inductor (LRES: A, B) are used to heat the filaments of the lamp during preheat and dimming, and also separate the lamp current from the filament current allowing for a single current-sensing resistor (RCS) to be utilized for sensing the lamp current. The AC lamp current measurement across RCS is coupled to the DIM pin through a feedback capacitor and resistor (CFB and RFB). A potentiometer dimming input circuit is used (PDIM, RMIN, RMAX) to convert the potentiometer resistance to the dimming reference voltage for the IRS2530D through the DIM pin. Protection against ballast fault conditions (failure to strike, open filament, and low AC line/brown-out) are incorporated into the IRS2530D to further reduce compo-

nent count.

There is a clear need for simple and cost effective dimming solutions which take up the minimum of real estate and do not require a large number of components. The 8-pin IRS2530D offers the means to develop dimming circuits in a quick and unproblematic manner. Furthermore, it has the potential to bring dimming features to a broader spectrum of applications, thus allowing marked energy savings to be realized.

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